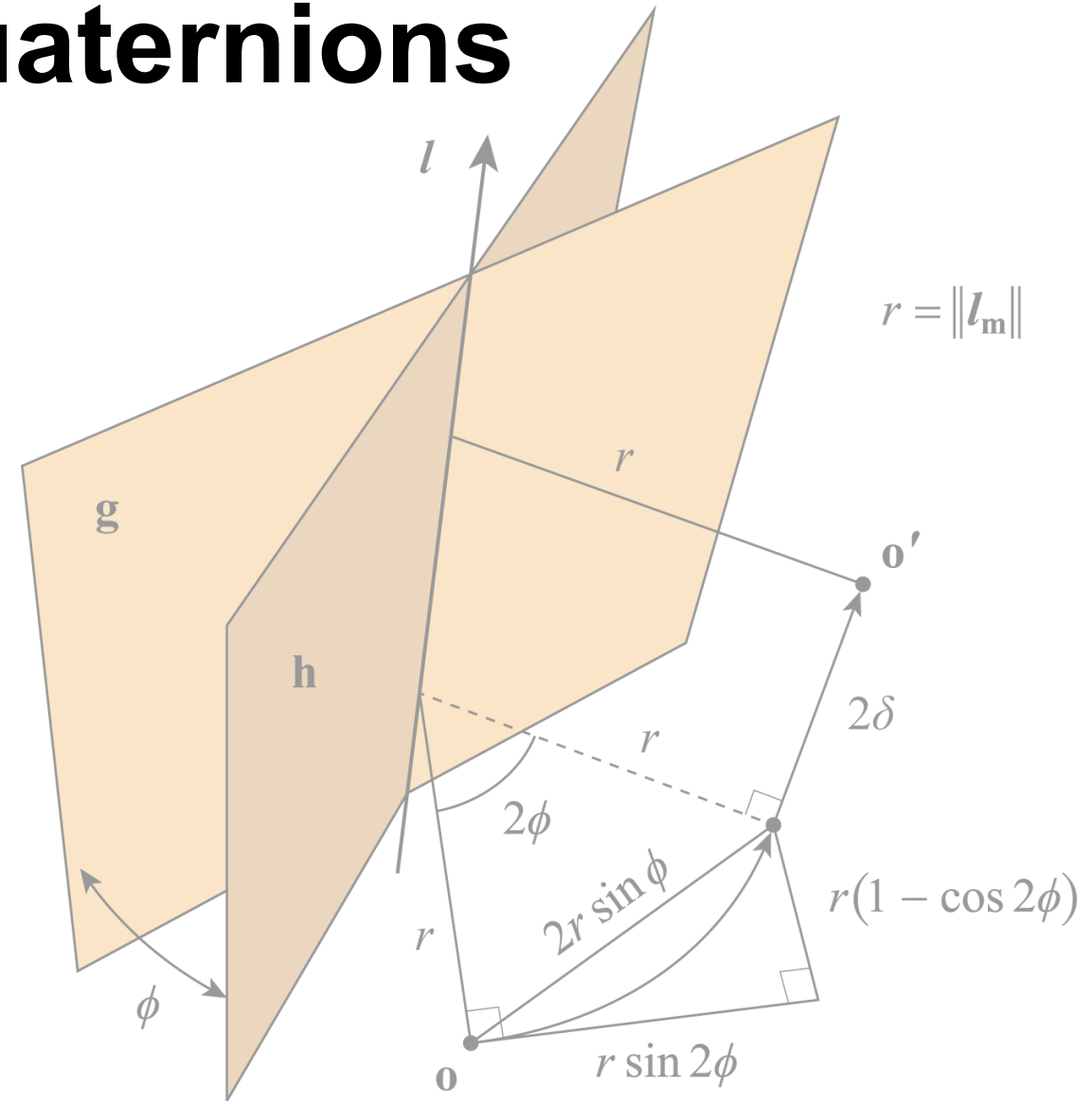
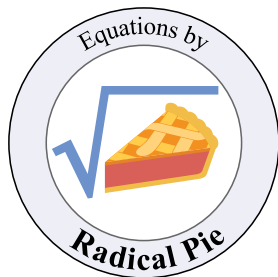


Projective Geometric Algebra and Relativistic Quaternions

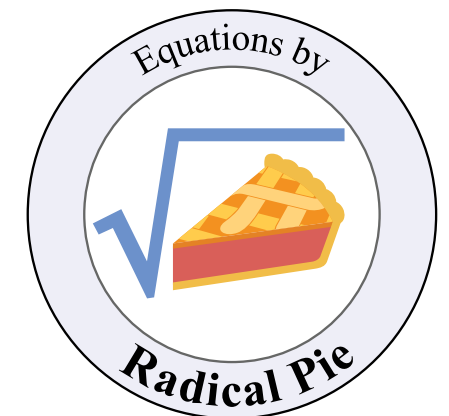
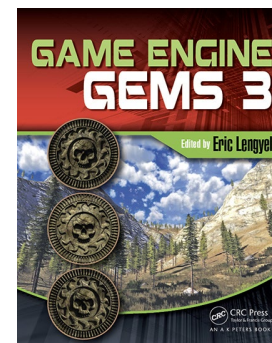
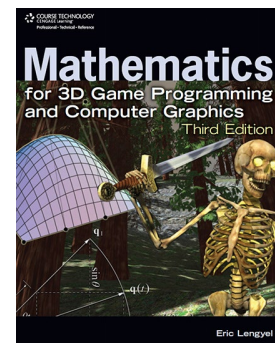
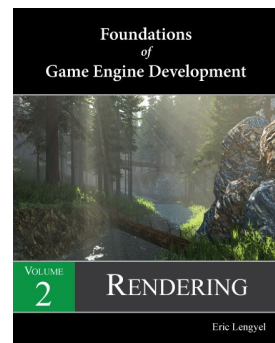
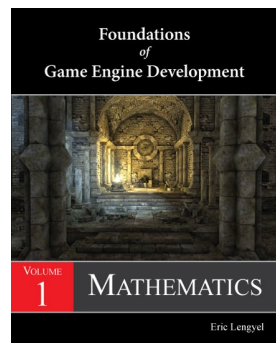
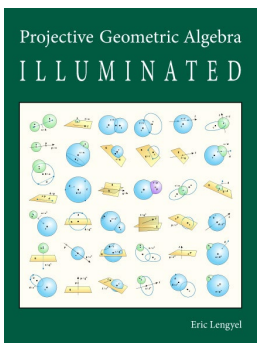
Eric Lengyel, Ph.D.

Virginia Tech
April 21, 2026



About the Speaker

- Virginia Tech mathematics alumnus, B.S. 1994, M.S. 1996
- UC Davis computer science, Ph.D. 2010
- Working in industry since 1994 (former Sierra, Apple, Sony)
- Developing algebraic models for about 15 years
- Occasionally teaches computer graphics
- Writes books about math and real-time rendering
- Mathematical typography expert



A Vast Subject Area

- No hope of covering all the fundamentals in one hour
- This talk is an introduction that paints the big picture

Projective Geometric Algebra

projectivegeometricalgebra.org

Basic Elements

Type	Values	Grade / Antigrade
Scalar	1	0/4
Vectors	e_1, e_2, e_3	1/3
Bivectors	$e_{12} = e_1 \wedge e_2, e_{13} = e_1 \wedge e_3, e_{23} = e_2 \wedge e_3$	2/2
Trivectors / Antivectors	$e_{123} = e_1 \wedge e_2 \wedge e_3$	3/1
Antiscalar	$\mathbb{I} = e_1 \wedge e_2 \wedge e_3, e_4$	4/0

Metric

Operation	Description	Identities
\bar{u}	Right complement of u	$u \wedge \bar{u} = 1, u \vee \bar{u} = 1$
\underline{u}	Left complement of u	$\bar{u} \wedge u = 1, \bar{u} \vee u = 1$
$u \bullet = \bar{G}u$	Bulk of u	$u \bullet = u \bullet$
$u \circ = \underline{G}u$	Weight of u	$u \circ = (e_1 \wedge u) \vee \bar{e}_1$
$u^* = \bar{G}u$	Right bulk dual of u	$u^* = \bar{u} \bullet, u^* \bullet = 0 \wedge 1$
$u^{\circ} = \underline{G}u$	Right weight dual of u	$u^{\circ} = \bar{u} \circ, u^{\circ} \circ = u \vee 1$
$u_{\bullet} = \bar{G}u$	Left bulk dual of u	$u_{\bullet} = \bar{u} \bullet, u_{\bullet} = \bar{1} \wedge u$
$u_{\circ} = \underline{G}u$	Left weight dual of u	$u_{\circ} = \bar{u} \circ, u_{\circ} = 1 \vee u$
\bar{u}	Reverse of u	$\bar{\bar{u}} = u, \bar{1} = -1, \bar{e}_i = -e_i$
\underline{u}	Antireverse of u	$\underline{\underline{u}} = u, \underline{\underline{1}} = -1, \underline{\underline{e}}_i = e_i$

Unary Operations

Operation	Description	Identities
\bar{u}	Right complement of u	$u \wedge \bar{u} = 1, u \vee \bar{u} = 1$
\underline{u}	Left complement of u	$\bar{u} \wedge u = 1, \bar{u} \vee u = 1$
$u \bullet = \bar{G}u$	Bulk of u	$u \bullet = u \bullet$
$u \circ = \underline{G}u$	Weight of u	$u \circ = (e_1 \wedge u) \vee \bar{e}_1$
$u^* = \bar{G}u$	Right bulk dual of u	$u^* = \bar{u} \bullet, u^* \bullet = 0 \wedge 1$
$u^{\circ} = \underline{G}u$	Right weight dual of u	$u^{\circ} = \bar{u} \circ, u^{\circ} \circ = u \vee 1$
$u_{\bullet} = \bar{G}u$	Left bulk dual of u	$u_{\bullet} = \bar{u} \bullet, u_{\bullet} = \bar{1} \wedge u$
$u_{\circ} = \underline{G}u$	Left weight dual of u	$u_{\circ} = \bar{u} \circ, u_{\circ} = 1 \vee u$
\bar{u}	Reverse of u	$\bar{\bar{u}} = u, \bar{1} = -1, \bar{e}_i = -e_i$
\underline{u}	Antireverse of u	$\underline{\underline{u}} = u, \underline{\underline{1}} = -1, \underline{\underline{e}}_i = e_i$

Binary Operations

Operation	Description	Identities
$a \wedge b$	Exterior product Wedge product "a wedge" b	$a \wedge b = \bar{b} \vee a$ $a \wedge b = \bar{b} \wedge a$
$a \vee b$	Exterior antiproduct Antiwedge product "a antivedge" b	$a \vee b = (-1)^{p(q+1)} b \wedge a$ $a \vee b = (-1)^{q(p+1)} b \vee a$
$a \cdot b$	Inner product Dot product "a dot" b	$a \cdot b = \bar{a} \wedge b$ $a \cdot b = \bar{a} \wedge b$
$a \bullet b$	Inner antiproduct Antidot product "a antidot" b	$a \bullet b = b \wedge a$ $a \bullet b = b \wedge a$
$a \Delta b$	Geometric product "a wedge-dot" b Identity is scalar 1	$a \Delta b = \bar{b} \vee a$ $a \Delta b = \bar{b} \wedge a$
$a \nabla b$	Geometric antiproduct "a antivedge-dot" b Identity is antiscalar 1	$a \nabla b = \bar{b} \vee a$ $a \nabla b = \bar{b} \wedge a$
$a \vee b^*$	Bulk contraction	$a \vee (b \wedge c)^* = a \vee b^* \vee c^*$ $a \vee (b \wedge c)^* = a \bullet b^* \wedge c^*$
$a \vee b^{\circ}$	Weight contraction	$a \vee b^{\circ} = a \bullet b$ when $g(a) = g(b)$
$a \wedge b^*$	Bulk expansion	$a \wedge b^* = a \bullet b$ when $g(a) = g(b)$
$a \wedge b^{\circ}$	Weight expansion	$a \wedge b^{\circ} = a \bullet b$ when $g(a) = g(b)$

Norms

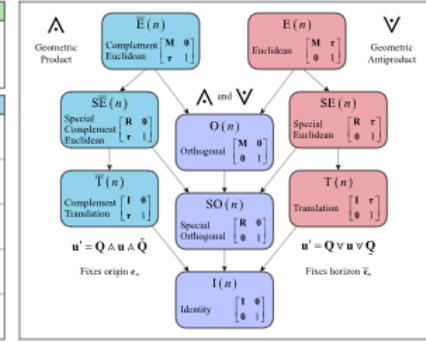
Definition	Description	Definition
$\ u\ _w = \sqrt{u \bullet u}$	Bulk norm of u	$\ u\ _w = \sqrt{u \bullet u} = \sqrt{u \wedge u^*}$
$\ u\ _o = \sqrt{u \circ u}$	Weight norm of u	$\ u\ _o = \sqrt{u \circ u} = \sqrt{u \vee u^{\circ}}$
$\ u\ = \sqrt{u \Delta u}$	Geometric norm of u	Projected geometric norm of u

Type	Projected Geometric Norm	Interpretation
Point p	$\ p\ = \sqrt{p^2 + p_3^2}$	Distance from origin to point p . Half distance that origin is moved by vector p .
Line l	$\ l\ = \frac{ l_3 }{\sqrt{l_1^2 + l_2^2}}$	Perpendicular distance from origin to line l . Half distance that origin is moved by motor l .
Plane g	$\ g\ = \frac{ g_3 }{\sqrt{g_1^2 + g_2^2}}$	Perpendicular distance from origin to plane g . Half distance that origin is moved by reflector g .
Motor Q	$\ Q\ = \sqrt{\frac{Q_0^2 + Q_1^2 + Q_2^2 + Q_3^2}{Q_4^2 + Q_5^2 + Q_6^2 + Q_7^2}}$	Half distance that origin is moved by motor Q .
Reflector F	$\ F\ = \sqrt{\frac{F_0^2 + F_1^2 + F_2^2 + F_3^2}{F_4^2 + F_5^2 + F_6^2 + F_7^2}}$	Half distance that origin is moved by reflector F .

Euclidean Measurements

Distance of Between Objects	Cosine of Angle ϕ Between Objects
$d(a, b) = \sqrt{ a \wedge b }$	$\cos \phi(a, b) = \frac{a \bullet b}{\ a\ \ b\ }$
$d(a, b, l) = \sqrt{ a \wedge b \wedge l }$	$\cos \phi(a, b, l) = \frac{a \bullet b \bullet l}{\ a\ \ b\ \ l\ }$

Transformation Groups



Distance Formula	Illustration
Distance d between points p and q .	
Perpendicular distance d between point p and line l .	
Perpendicular distance d between point p and plane g .	
Perpendicular distance d between skew lines l and k .	

Angle Formula	Illustration
Cosine of angle ϕ between planes g and h .	
Cosine of angle ϕ between plane g and line l .	
Cosine of angle ϕ between lines l and k .	

DISTANCE

ANGLE

Point p (Vector)

OD

Position: $p = p_1 e_1 + p_2 e_2 + p_3 e_3$

Weight: $\bar{p} = p_1 \bar{e}_1 + p_2 \bar{e}_2 + p_3 \bar{e}_3$

Bulk: $\bar{p} \bullet = p_1 \bar{e}_1 + p_2 \bar{e}_2 + p_3 \bar{e}_3$

Weight dual: $\bar{p}^{\circ} = p_1 \bar{e}_1 + p_2 \bar{e}_2 + p_3 \bar{e}_3$

Bulk dual: $\bar{p}^{\bullet} = p_1 \bar{e}_1 + p_2 \bar{e}_2 + p_3 \bar{e}_3$

Weight dual: $\bar{p}^{\circ} = p_1 \bar{e}_1 + p_2 \bar{e}_2 + p_3 \bar{e}_3$

Bulk norm: $\|\bar{p}\|_w = \sqrt{p_1^2 + p_2^2 + p_3^2}$

Weight norm: $\|\bar{p}\|_o = |p_3|$

Altitude: $\text{alt}(p) = p \bullet e_3 = p_3$

Right complement: $\bar{p} = p_1 \bar{e}_1 + p_2 \bar{e}_2 + p_3 \bar{e}_3$

Degrees of freedom: $\text{DOF}(3, 0) = 3$

Line l (Bivector)

1D

Direction: $l = l_1 e_1 \wedge e_2 + l_2 e_1 \wedge e_3 + l_3 e_2 \wedge e_3$

Moment: $\bar{l} = l_1 \bar{e}_1 \wedge \bar{e}_2 + l_2 \bar{e}_1 \wedge \bar{e}_3 + l_3 \bar{e}_2 \wedge \bar{e}_3$

Bulk: $\bar{l} \bullet = l_1 \bar{e}_1 \wedge \bar{e}_2 + l_2 \bar{e}_1 \wedge \bar{e}_3 + l_3 \bar{e}_2 \wedge \bar{e}_3$

Weight: $\bar{l} \circ = l_1 \bar{e}_1 \wedge \bar{e}_2 + l_2 \bar{e}_1 \wedge \bar{e}_3 + l_3 \bar{e}_2 \wedge \bar{e}_3$

Bulk dual: $\bar{l}^{\bullet} = l_1 \bar{e}_1 \wedge \bar{e}_2 + l_2 \bar{e}_1 \wedge \bar{e}_3 + l_3 \bar{e}_2 \wedge \bar{e}_3$

Weight dual: $\bar{l}^{\circ} = l_1 \bar{e}_1 \wedge \bar{e}_2 + l_2 \bar{e}_1 \wedge \bar{e}_3 + l_3 \bar{e}_2 \wedge \bar{e}_3$

Bulk norm: $\|\bar{l}\|_w = \sqrt{l_1^2 + l_2^2 + l_3^2}$

Weight norm: $\|\bar{l}\|_o = |l_3|$

Altitude: $\text{alt}(l) = l \vee e_3 = l_3 e_1 \wedge e_2$

Right complement: $\bar{l} = l_1 \bar{e}_1 \wedge \bar{e}_2 + l_2 \bar{e}_1 \wedge \bar{e}_3 + l_3 \bar{e}_2 \wedge \bar{e}_3$

Degrees of freedom: $\text{DOF}(3, 1) = 4$

Constraints: $l_1, l_2 = 0$

Plane g (Trivector)

2D

Normal: $g = g_1 e_1 \wedge e_2 \wedge e_3$

Position: $\bar{g} = g_1 \bar{e}_1 \wedge \bar{e}_2 \wedge \bar{e}_3$

Bulk: $\bar{g} \bullet = g_1 \bar{e}_1 \wedge \bar{e}_2 \wedge \bar{e}_3$

Weight: $\bar{g} \circ = g_1 \bar{e}_1 \wedge \bar{e}_2 \wedge \bar{e}_3$

Bulk dual: $\bar{g}^{\bullet} = g_1 \bar{e}_1 \wedge \bar{e}_2 \wedge \bar{e}_3$

Weight dual: $\bar{g}^{\circ} = g_1 \bar{e}_1 \wedge \bar{e}_2 \wedge \bar{e}_3$

Bulk norm: $\|\bar{g}\|_w = |g_1|$

Weight norm: $\|\bar{g}\|_o = \sqrt{g_1^2}$

Altitude: $\text{alt}(g) = g \vee e_3 = g_1 e_1 \wedge e_2$

Right complement: $\bar{g} = g_1 \bar{e}_1 \wedge \bar{e}_2 \wedge \bar{e}_3$

Degrees of freedom: $\text{DOF}(3, 2) = 3$

Geometric Product $a \Delta b$

$a \backslash b$	1	e_1	e_2	e_3	e_{12}	e_{13}	e_{23}	\mathbb{I}
1	1	0	0	0	0	0	0	0
e_1	0	1	0	0	0	0	0	0
e_2	0	0	1	0	0	0	0	0
e_3	0	0	0	1	0	0	0	0
e_{12}	0	0	0	0	1	0	0	0
e_{13}	0	0	0	0	0	1	0	0
e_{23}	0	0	0	0	0	0	1	0
\mathbb{I}	0	0	0	0	0	0	0	1

JOIN

Join Operation	Illustration
Line containing points p and q . $p \Delta q = (p_1 q_2 - p_2 q_1) e_1 + (p_1 q_3 - p_3 q_1) e_2 + (p_2 q_3 - p_3 q_2) e_3$	
Plane containing line l and point p . $l \Delta p = (l_1 p_2 - l_2 p_1) e_{12} + (l_1 p_3 - l_3 p_1) e_{13} + (l_2 p_3 - l_3 p_2) e_{23}$	

MEET

Meet Operation	Illustration
Line where planes g and h intersect. $g \vee h = (g_1 h_2 - g_2 h_1) e_1 + (g_1 h_3 - g_3 h_1) e_2 + (g_2 h_3 - g_3 h_2) e_3$	
Point where plane g and line l intersect. $g \vee l = (g_1 l_2 - g_2 l_1) e_1 + (g_1 l_3 - g_3 l_1) e_2 + (g_2 l_3 - g_3 l_2) e_3$	

EXPANSION

Expansion Operation	Illustration
Line containing point p and orthogonal to plane g . $p \Delta g^{\circ} = (p_1 g_2 - p_2 g_1) e_1 + (p_1 g_3 - p_3 g_1) e_2 + (p_2 g_3 - p_3 g_2) e_3$	
Plane containing point p and orthogonal to line l . $p \Delta l^{\circ} = (p_1 l_2 - p_2 l_1) e_{12} + (p_1 l_3 - p_3 l_1) e_{13} + (p_2 l_3 - p_3 l_2) e_{23}$	
Plane containing line l and orthogonal to plane g . $l \Delta g^{\circ} = (l_1 g_2 - l_2 g_1) e_{12} + (l_1 g_3 - l_3 g_1) e_{13} + (l_2 g_3 - l_3 g_2) e_{23}$	

PROJECTION

Projection Operation	Illustration
Orthogonal projection of point p onto plane g . $g \vee (p \Delta g^{\circ}) = (g_1^2 + g_2^2 + g_3^2)(p_1 e_1 + p_2 e_2 + p_3 e_3) - (g_1 p_2 - g_2 p_1) e_3 - (g_1 p_3 - g_3 p_1) e_2 - (g_2 p_3 - g_3 p_2) e_1$	
Orthogonal projection of point p onto line l . $l \vee (p \Delta l^{\circ}) = (l_1^2 + l_2^2 + l_3^2)(p_1 e_1 + p_2 e_2 + p_3 e_3) + (l_1 p_2 - l_2 p_1) e_3 + (l_1 p_3 - l_3 p_1) e_2 + (l_2 p_3 - l_3 p_2) e_1$	
Orthogonal projection of line l onto plane g . $g \vee (l \Delta g^{\circ}) = (g_1^2 + g_2^2 + g_3^2)(l_1 e_1 + l_2 e_2 + l_3 e_3) - (g_1 l_2 - g_2 l_1) e_3 - (g_1 l_3 - g_3 l_1) e_2 - (g_2 l_3 - g_3 l_2) e_1$	
Central projection of point p onto plane g . $g \vee (p \Delta g^{\circ}) = g_1^2(p_1 e_1 + p_2 e_2 + p_3 e_3) - (g_1 p_2 - g_2 p_1) e_3 - (g_1 p_3 - g_3 p_1) e_2 - (g_2 p_3 - g_3 p_2) e_1$	
Central projection of point p onto line l . $l \vee (p \Delta l^{\circ}) = (l_1^2 + l_2^2 + l_3^2)(p_1 e_1 + p_2 e_2 + p_3 e_3) + (l_1 p_2 - l_2 p_1) e_3 + (l_1 p_3 - l_3 p_1) e_2 + (l_2 p_3 - l_3 p_2) e_1$	
Central projection of line l onto plane g . $g \vee (l \Delta g^{\circ}) = (g_1^2 + g_2^2 + g_3^2)(l_1 e_1 + l_2 e_2 + l_3 e_3) - (g_1 l_2 - g_2 l_1) e_3 - (g_1 l_3 - g_3 l_1) e_2 - (g_2 l_3 - g_3 l_2) e_1$	

Motor Q Motion Operator

$Q = Q_0 e_1 + Q_1 e_2 + Q_2 e_3 + Q_3 \mathbb{I} + Q_4 e_{12} + Q_5 e_{13} + Q_6 e_{23} + Q_7 \mathbb{I}$

Rotation: $Q = \exp(\theta \mathbb{I}) = \cos(\theta/2) + \sin(\theta/2) \mathbb{I}$

Moment and Displacement: $Q = \exp(\theta \mathbb{I} + \delta l) = \cos(\theta/2 + \delta l) + \sin(\theta/2 + \delta l) \mathbb{I} + \delta l$

$Q \vee v \vee Q$ rotates object v through angle θ about unit axis l and translates by distance δl along direction of line l .

Matrix conversion	$M_Q = A_Q + B_Q$	$M'_Q = A_Q - B_Q$
A_Q	$\begin{bmatrix} 1-2(Q_4^2+Q_5^2) & 2Q_4 Q_1 & 2Q_4 Q_2 & 2(Q_4 Q_3-Q_5 Q_6) \\ 2Q_4 Q_1 & 1-2(Q_4^2+Q_5^2) & 2Q_4 Q_3 & 2(Q_4 Q_6-Q_5 Q_7) \\ 2Q_4 Q_2 & 2Q_4 Q_3 & 1-2(Q_4^2+Q_5^2) & 2(Q_4 Q_7-Q_5 Q_8) \\ 2Q_4 Q_3 & 2Q_4 Q_6 & 2Q_4 Q_7 & 1-2(Q_4^2+Q_5^2) \end{bmatrix}$	$\begin{bmatrix} 1-2(Q_6^2+Q_7^2) & 2Q_6 Q_1 & 2Q_6 Q_2 & 2(Q_6 Q_3-Q_7 Q_4) \\ 2Q_6 Q_1 & 1-2(Q_6^2+Q_7^2) & 2Q_6 Q_5 & 2(Q_6 Q_8-Q_7 Q_9) \\ 2Q_6 Q_2 & 2Q_6 Q_5 & 1-2(Q_6^2+Q_7^2) & 2(Q_6 Q_{10}-Q_7 Q_{11}) \\ 2Q_6 Q_3 & 2Q_6 Q_8 & 2Q_6 Q_{10} & 1-2(Q_6^2+Q_7^2) \end{bmatrix}$

Reflector F

$F = F_0 e_1 + F_1 e_2 + F_2 e_3 + F_3 \mathbb{I} + F_4 e_{12} + F_5 e_{13} + F_6 e_{23} + F_7 \mathbb{I}$

Point: $F = p \bullet = p_1 \bar{e}_1 + p_2 \bar{e}_2 + p_3 \bar{e}_3$

Plane: $F = g \bullet = g_1 \bar{e}_1 \wedge \bar{e}_2 \wedge \bar{e}_3$

$F \vee v \vee F$ reflects object v across plane g .

Matrix conversion	$M_F = A_F + B_F$	$M'_F = A_F - B_F$
A_F	$\begin{bmatrix} 1-F_4^2-F_5^2 & -2F_4 F_1 & -2F_4 F_2 & 2(F_4 F_3-F_5 F_6) \\ -2F_4 F_1 & 1-F_4^2-F_5^2 & -2F_4 F_3 & 2(F_4 F_6-F_5 F_7) \\ -2F_4 F_2 & -2F_4 F_3 & 1-F_4^2-F_5^2 & 2(F_4 F_7-F_5 F_8) \\ -2F_4 F_3 & -2F_4 F_6 & -2F_4 F_7 & 1-F_4^2-F_5^2 \end{bmatrix}$	$\begin{bmatrix} 1-F_6^2-F_7^2 & -2F_6 F_1 & -2F_6 F_2 & 2(F_6 F_3-F_7 F_4) \\ -2F_6 F_1 & 1-F_6^2-F_7^2 & -2F_6 F_5 & 2(F_6 F_8-F_7 F_9) \\ -2F_6 F_2 & -2F_6 F_5 & 1-F_6^2-F_7^2 & 2(F_6 F_{10}-F_7 F_{11}) \\ -2F_6 F_3 & -2F_6 F_8 & -2F_6 F_{10} & 1-F_6^2-F_7^2 \end{bmatrix}$

Conformal Geometric Algebra

conformalgeometricalgebra.org

JOIN

Join Operation	Illustration
<p>Dipole containing round point a and b</p> $\mathbf{a} \wedge \mathbf{b} = (a_1 b_2 - a_2 b_1) \mathbf{e}_{12} + (a_2 b_3 - a_3 b_2) \mathbf{e}_{23} + (a_3 b_1 - a_1 b_3) \mathbf{e}_{31}$ $+ (a_1 b_2 - a_2 b_1) \mathbf{e}_{12} + (a_2 b_3 - a_3 b_2) \mathbf{e}_{23} + (a_3 b_1 - a_1 b_3) \mathbf{e}_{31}$	
<p>Line containing flat point p and round point a</p> $\mathbf{p} \wedge \mathbf{a} = (p_1 a_2 - p_2 a_1) \mathbf{e}_{12} + (p_2 a_3 - p_3 a_2) \mathbf{e}_{23} + (p_3 a_1 - p_1 a_3) \mathbf{e}_{31}$	
<p>Circle containing dipole d and round point a</p> $\mathbf{d} \wedge \mathbf{a} = (d_1 a_2 - d_2 a_1) \mathbf{e}_{12} + (d_2 a_3 - d_3 a_2) \mathbf{e}_{23} + (d_3 a_1 - d_1 a_3) \mathbf{e}_{31}$	
<p>Plane containing line l and round point a</p> $\mathbf{l} \wedge \mathbf{a} = (l_1 a_2 - l_2 a_1) \mathbf{e}_{12} + (l_2 a_3 - l_3 a_2) \mathbf{e}_{23} + (l_3 a_1 - l_1 a_3) \mathbf{e}_{31}$	
<p>Plane containing dipole d and flat point p</p> $\mathbf{d} \wedge \mathbf{p} = (d_1 p_2 - d_2 p_1) \mathbf{e}_{12} + (d_2 p_3 - d_3 p_2) \mathbf{e}_{23} + (d_3 p_1 - d_1 p_3) \mathbf{e}_{31}$	
<p>Sphere containing circle c and round point a</p> $\mathbf{c} \wedge \mathbf{a} = (c_1 a_2 - c_2 a_1) \mathbf{e}_{12} + (c_2 a_3 - c_3 a_2) \mathbf{e}_{23} + (c_3 a_1 - c_1 a_3) \mathbf{e}_{31}$	
<p>Sphere containing dipole d and l</p> $\mathbf{d} \wedge \mathbf{l} = (d_1 l_2 - d_2 l_1) \mathbf{e}_{12} + (d_2 l_3 - d_3 l_2) \mathbf{e}_{23} + (d_3 l_1 - d_1 l_3) \mathbf{e}_{31}$	

Meet Operation	Illustration
<p>Circle where spheres s and l intersect</p> $\mathbf{s} \vee \mathbf{l} = (s_1 l_2 - l_2 s_1) \mathbf{e}_{12} + (s_2 l_3 - l_3 s_2) \mathbf{e}_{23} + (s_3 l_1 - l_1 s_3) \mathbf{e}_{31}$	
<p>Circle where sphere s and plane g intersect</p> $\mathbf{s} \vee \mathbf{g} = (s_1 g_2 - g_2 s_1) \mathbf{e}_{12} + (s_2 g_3 - g_3 s_2) \mathbf{e}_{23} + (s_3 g_1 - g_1 s_3) \mathbf{e}_{31}$	
<p>Line where planes g and h intersect</p> $\mathbf{g} \vee \mathbf{h} = (g_1 h_2 - h_2 g_1) \mathbf{e}_{12} + (g_2 h_3 - h_3 g_2) \mathbf{e}_{23} + (g_3 h_1 - h_1 g_3) \mathbf{e}_{31}$	
<p>Dipole where sphere s and circle c intersect</p> $\mathbf{s} \vee \mathbf{c} = (s_1 c_2 - c_2 s_1) \mathbf{e}_{12} + (s_2 c_3 - c_3 s_2) \mathbf{e}_{23} + (s_3 c_1 - c_1 s_3) \mathbf{e}_{31}$	
<p>Dipole where plane g and circle c intersect</p> $\mathbf{g} \vee \mathbf{c} = (g_1 c_2 - c_2 g_1) \mathbf{e}_{12} + (g_2 c_3 - c_3 g_2) \mathbf{e}_{23} + (g_3 c_1 - c_1 g_3) \mathbf{e}_{31}$	
<p>Round point contained in flat point p and contained by sphere s</p> $\mathbf{p} \vee \mathbf{s} = (p_1 s_2 - s_2 p_1) \mathbf{e}_{12} + (p_2 s_3 - s_3 p_2) \mathbf{e}_{23} + (p_3 s_1 - s_1 p_3) \mathbf{e}_{31}$	

EXPANSION	
<p>Dipole containing round point a and orthogonal to sphere s</p> $\mathbf{a} \wedge \mathbf{s} = (a_1 s_2 - s_2 a_1) \mathbf{e}_{12} + (a_2 s_3 - s_3 a_2) \mathbf{e}_{23} + (a_3 s_1 - s_1 a_3) \mathbf{e}_{31}$	
<p>Dipole containing round point a and orthogonal to plane p</p> $\mathbf{a} \wedge \mathbf{p} = (a_1 p_2 - p_2 a_1) \mathbf{e}_{12} + (a_2 p_3 - p_3 a_2) \mathbf{e}_{23} + (a_3 p_1 - p_1 a_3) \mathbf{e}_{31}$	
<p>Circle containing dipole d and orthogonal to sphere s</p> $\mathbf{d} \wedge \mathbf{s} = (d_1 s_2 - s_2 d_1) \mathbf{e}_{12} + (d_2 s_3 - s_3 d_2) \mathbf{e}_{23} + (d_3 s_1 - s_1 d_3) \mathbf{e}_{31}$	
<p>Circle containing dipole d and orthogonal to plane p</p> $\mathbf{d} \wedge \mathbf{p} = (d_1 p_2 - p_2 d_1) \mathbf{e}_{12} + (d_2 p_3 - p_3 d_2) \mathbf{e}_{23} + (d_3 p_1 - p_1 d_3) \mathbf{e}_{31}$	
<p>Line containing flat point p and orthogonal to sphere s</p> $\mathbf{p} \wedge \mathbf{s} = (p_1 s_2 - s_2 p_1) \mathbf{e}_{12} + (p_2 s_3 - s_3 p_2) \mathbf{e}_{23} + (p_3 s_1 - s_1 p_3) \mathbf{e}_{31}$	
<p>Line containing flat point p and orthogonal to plane p</p> $\mathbf{p} \wedge \mathbf{p} = (p_1 p_2 - p_2 p_1) \mathbf{e}_{12} + (p_2 p_3 - p_3 p_2) \mathbf{e}_{23} + (p_3 p_1 - p_1 p_3) \mathbf{e}_{31}$	

Meet Operation	Illustration
<p>Dipole where sphere s and line l intersect</p> $\mathbf{s} \vee \mathbf{l} = (s_1 l_2 - l_2 s_1) \mathbf{e}_{12} + (s_2 l_3 - l_3 s_2) \mathbf{e}_{23} + (s_3 l_1 - l_1 s_3) \mathbf{e}_{31}$	
<p>Flat point where plane g and line l intersect</p> $\mathbf{g} \vee \mathbf{l} = (g_1 l_2 - l_2 g_1) \mathbf{e}_{12} + (g_2 l_3 - l_3 g_2) \mathbf{e}_{23} + (g_3 l_1 - l_1 g_3) \mathbf{e}_{31}$	
<p>Round point contained by circle c and s</p> $\mathbf{c} \vee \mathbf{s} = (c_1 s_2 - s_2 c_1) \mathbf{e}_{12} + (c_2 s_3 - s_3 c_2) \mathbf{e}_{23} + (c_3 s_1 - s_1 c_3) \mathbf{e}_{31}$	
<p>Round point contained in line l and contained by circle c</p> $\mathbf{l} \vee \mathbf{c} = (l_1 c_2 - c_2 l_1) \mathbf{e}_{12} + (l_2 c_3 - c_3 l_2) \mathbf{e}_{23} + (l_3 c_1 - c_1 l_3) \mathbf{e}_{31}$	
<p>Round point contained by sphere s and dipole d</p> $\mathbf{s} \vee \mathbf{d} = (s_1 d_2 - d_2 s_1) \mathbf{e}_{12} + (s_2 d_3 - d_3 s_2) \mathbf{e}_{23} + (s_3 d_1 - d_1 s_3) \mathbf{e}_{31}$	
<p>Round point contained in plane p and contained by dipole d</p> $\mathbf{p} \vee \mathbf{d} = (p_1 d_2 - d_2 p_1) \mathbf{e}_{12} + (p_2 d_3 - d_3 p_2) \mathbf{e}_{23} + (p_3 d_1 - d_1 p_3) \mathbf{e}_{31}$	

Flat Point p (Bivector)	Flat Line l (Trivector)	Flat Plane g (Quadrivector)
$\mathbf{p} = p_1 \mathbf{e}_{12} + p_2 \mathbf{e}_{23} + p_3 \mathbf{e}_{31}$	$\mathbf{l} = l_1 \mathbf{e}_{123} + l_2 \mathbf{e}_{231} + l_3 \mathbf{e}_{312}$	$\mathbf{g} = g_1 \mathbf{e}_{1234} + g_2 \mathbf{e}_{2341} + g_3 \mathbf{e}_{3412} + g_4 \mathbf{e}_{4123}$
<p>Dual</p> $\mathbf{p}^* = p_2 \mathbf{e}_{31} - p_3 \mathbf{e}_{12} + p_1 \mathbf{e}_{23}$	<p>Dual</p> $\mathbf{l}^* = l_2 \mathbf{e}_{31} + l_3 \mathbf{e}_{12} + l_1 \mathbf{e}_{23}$	<p>Dual</p> $\mathbf{g}^* = -g_2 \mathbf{e}_{41} - g_3 \mathbf{e}_{12} - g_4 \mathbf{e}_{23} + g_1 \mathbf{e}_{34}$
<p>Attitude</p> $\text{att}(\mathbf{p}) = \mathbf{p} \vee \mathbf{e}_{123}$	<p>Attitude</p> $\text{att}(\mathbf{l}) = \mathbf{l} \vee \mathbf{e}_{1234}$	<p>Attitude</p> $\text{att}(\mathbf{g}) = \mathbf{g} \vee \mathbf{e}_{1234}$
<p>Flat Bulk</p> $\mathbf{p} \wedge \mathbf{p} = p_1 p_2 \mathbf{e}_{123} + p_2 p_3 \mathbf{e}_{231} + p_3 p_1 \mathbf{e}_{312}$	<p>Flat Bulk</p> $\mathbf{l} \wedge \mathbf{l} = l_1 l_2 \mathbf{e}_{123} + l_2 l_3 \mathbf{e}_{231} + l_3 l_1 \mathbf{e}_{312}$	<p>Flat Bulk</p> $\mathbf{g} \wedge \mathbf{g} = g_1 g_2 \mathbf{e}_{1234} + g_2 g_3 \mathbf{e}_{2341} + g_3 g_4 \mathbf{e}_{3412} + g_4 g_1 \mathbf{e}_{4123}$
<p>Flat Weight</p> $ \mathbf{p} = \sqrt{p_1^2 + p_2^2 + p_3^2}$	<p>Flat Weight</p> $ \mathbf{l} = \sqrt{l_1^2 + l_2^2 + l_3^2}$	<p>Flat Weight</p> $ \mathbf{g} = \sqrt{g_1^2 + g_2^2 + g_3^2 + g_4^2}$
<p>Position Norm</p> $\frac{ \mathbf{p} }{ \mathbf{e}_{123} } = \sqrt{p_1^2 + p_2^2 + p_3^2}$	<p>Position Norm</p> $\frac{ \mathbf{l} }{ \mathbf{e}_{1234} } = \sqrt{l_1^2 + l_2^2 + l_3^2}$	<p>Position Norm</p> $\frac{ \mathbf{g} }{ \mathbf{e}_{1234} } = \sqrt{g_1^2 + g_2^2 + g_3^2 + g_4^2}$

Round Point a (Vector)	Sphere s (Quadrivector)
$\mathbf{a} = a_1 \mathbf{e}_1 + a_2 \mathbf{e}_2 + a_3 \mathbf{e}_3$	$\mathbf{s} = s_1 \mathbf{e}_{1234} + s_2 \mathbf{e}_{2341} + s_3 \mathbf{e}_{3412} + s_4 \mathbf{e}_{4123}$
<p>Dual</p> $\mathbf{a}^* = a_2 \mathbf{e}_{31} - a_3 \mathbf{e}_{12} + a_1 \mathbf{e}_{23}$	<p>Dual</p> $\mathbf{s}^* = -s_2 \mathbf{e}_{41} - s_3 \mathbf{e}_{12} - s_4 \mathbf{e}_{23} + s_1 \mathbf{e}_{34}$
<p>Attitude</p> $\text{att}(\mathbf{a}) = \mathbf{a} \vee \mathbf{e}_{123}$	<p>Attitude</p> $\text{att}(\mathbf{s}) = \mathbf{s} \vee \mathbf{e}_{1234}$
<p>Center Point</p> $\text{cen}(\mathbf{a}) = \mathbf{a}$	<p>Center</p> $\text{cen}(\mathbf{s}) = \text{att}(\mathbf{s}) \vee \mathbf{a}$
<p>Infinity</p> $\text{inf}(\mathbf{a}) = \mathbf{a} \wedge \mathbf{e}_{123}$	<p>Container</p> $\text{con}(\mathbf{s}) = \mathbf{s} \wedge \text{att}(\mathbf{s})^*$
<p>Carrier Plane</p> $\text{car}(\mathbf{a}) = \mathbf{a} \wedge \mathbf{e}_{123}$	<p>Carrier</p> $\text{car}(\mathbf{s}) = \mathbf{s} \wedge \mathbf{e}_{123}$
<p>Coariser</p> $\text{coar}(\mathbf{a}) = \mathbf{a} \wedge \mathbf{e}_{123}$	<p>Coariser</p> $\text{coar}(\mathbf{s}) = \mathbf{s} \wedge \mathbf{e}_{1234}$
<p>Round Bulk</p> $\mathbf{a} \wedge \mathbf{a} = 0$	<p>Round Bulk</p> $\mathbf{s} \wedge \mathbf{s} = 0$
<p>Round Weight</p> $ \mathbf{a} = \sqrt{a_1^2 + a_2^2 + a_3^2}$	<p>Round Weight</p> $ \mathbf{s} = \sqrt{s_1^2 + s_2^2 + s_3^2 + s_4^2}$
<p>Flat Bulk</p> $\mathbf{a} \wedge \mathbf{a} = 0$	<p>Flat Bulk</p> $\mathbf{s} \wedge \mathbf{s} = 0$
<p>Flat Weight</p> $ \mathbf{a} = 0$	<p>Flat Weight</p> $ \mathbf{s} = 0$

Dipole d (Bivector)	Carrier Line	Carrier Position	Carrier
$\mathbf{d} = d_1 \mathbf{e}_{12} + d_2 \mathbf{e}_{23} + d_3 \mathbf{e}_{31}$	$\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	$\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	$\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Center</p> $\text{cen}(\mathbf{d}) = \text{att}(\mathbf{d}) \vee \mathbf{a}$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Dual</p> $\mathbf{d}^* = d_2 \mathbf{e}_{31} - d_3 \mathbf{e}_{12} + d_1 \mathbf{e}_{23}$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Coariser</p> $\text{coar}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Round Bulk</p> $\mathbf{d} \wedge \mathbf{d} = 0$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Round Weight</p> $ \mathbf{d} = \sqrt{d_1^2 + d_2^2 + d_3^2}$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Flat Bulk</p> $\mathbf{d} \wedge \mathbf{d} = 0$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$
<p>Flat Weight</p> $ \mathbf{d} = 0$	<p>Carrier Line</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$	<p>Carrier Position</p> $\text{pos}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{d}) = \mathbf{d} \wedge \mathbf{e}_{123}$

Circle c (Trivector)	Carrier Plane	Carrier Moment	Carrier
$\mathbf{c} = c_1 \mathbf{e}_{123} + c_2 \mathbf{e}_{231} + c_3 \mathbf{e}_{312}$	$\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	$\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	$\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Center</p> $\text{cen}(\mathbf{c}) = \text{att}(\mathbf{c}) \vee \mathbf{a}$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Dual</p> $\mathbf{c}^* = c_2 \mathbf{e}_{31} + c_3 \mathbf{e}_{12} + c_1 \mathbf{e}_{23}$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Coariser</p> $\text{coar}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Round Bulk</p> $\mathbf{c} \wedge \mathbf{c} = 0$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Round Weight</p> $ \mathbf{c} = \sqrt{c_1^2 + c_2^2 + c_3^2}$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Flat Bulk</p> $\mathbf{c} \wedge \mathbf{c} = 0$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$
<p>Flat Weight</p> $ \mathbf{c} = 0$	<p>Carrier Plane</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier Moment</p> $\text{mom}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$	<p>Carrier</p> $\text{car}(\mathbf{c}) = \mathbf{c} \wedge \mathbf{e}_{1234}$

FLATS

ROUNDS

Grassmann / Clifford Algebras

- You've probably been using pieces of these algebras already without realizing it
- Cross products
- Homogeneous coordinates (x, y, z, w)
- Planes (a, b, c, d)
- Plücker coordinates
- Quaternions

Cross Products

- Units of distance become units of area

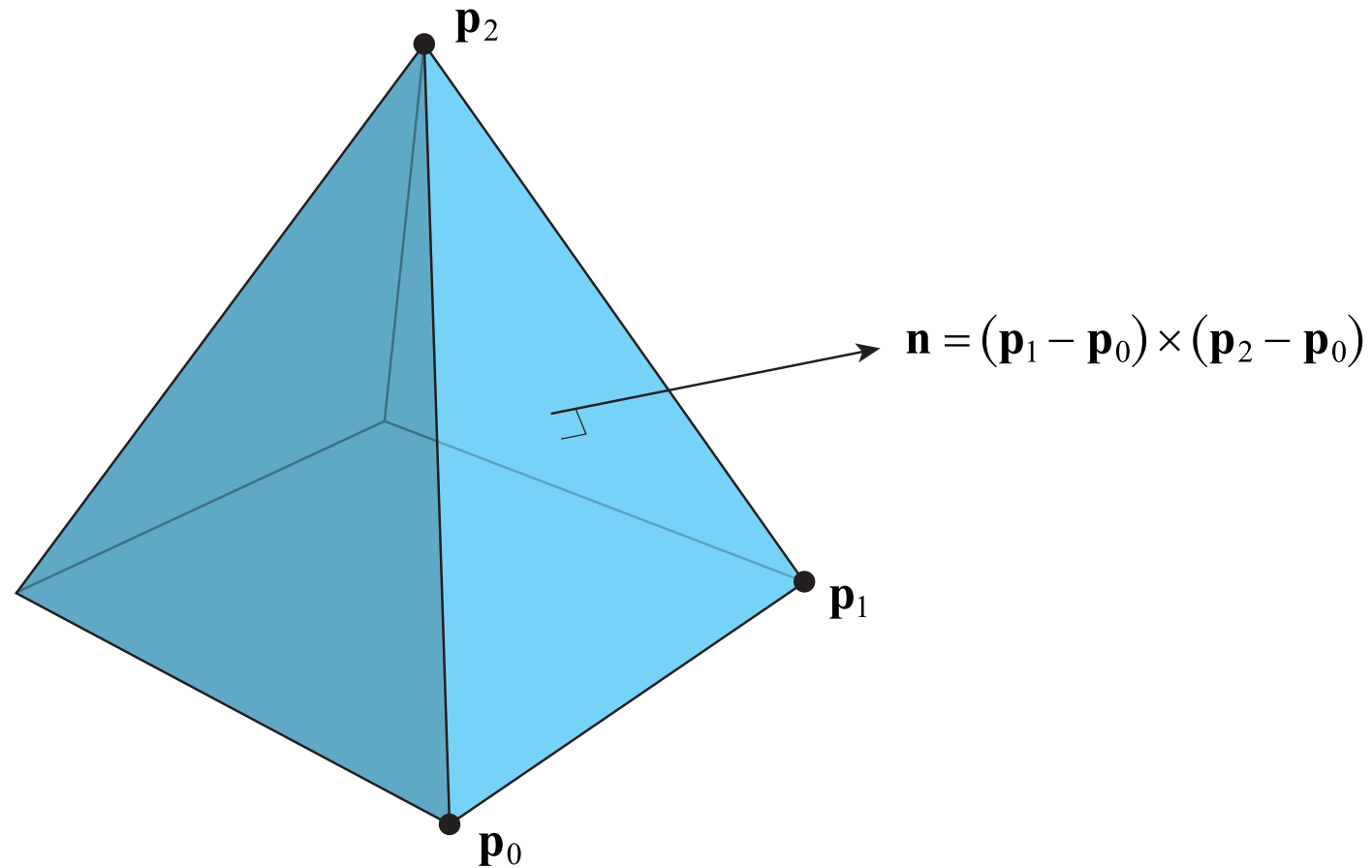
$$(a_x, a_y, a_z) \times (b_x, b_y, b_z)$$



$$(a_y b_z - a_z b_y, a_z b_x - a_x b_z, a_x b_y - a_y b_x)$$

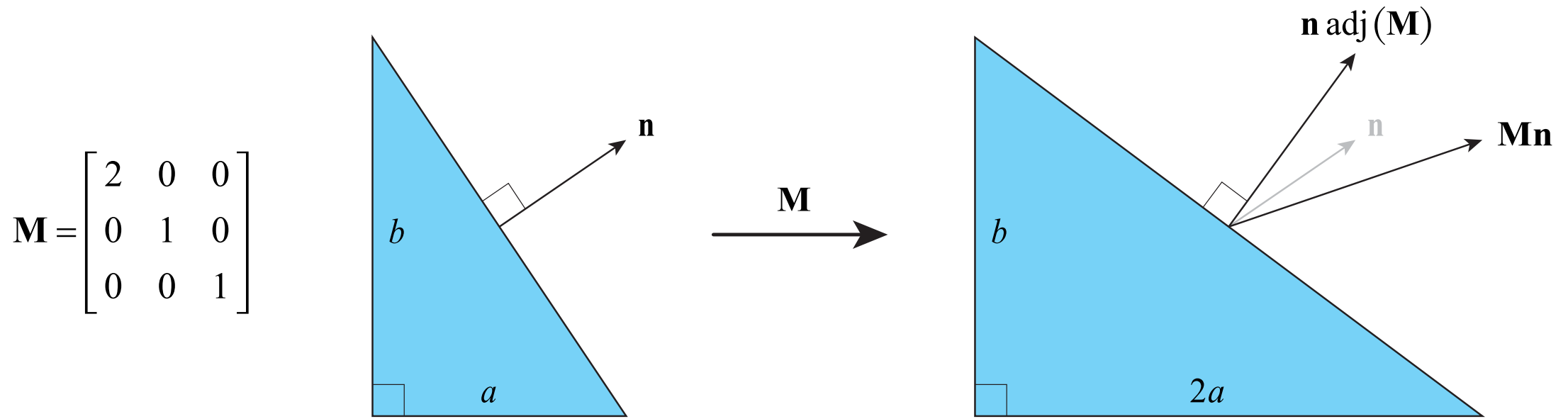
Normal Vectors

- Cross product calculates normal of triangular face



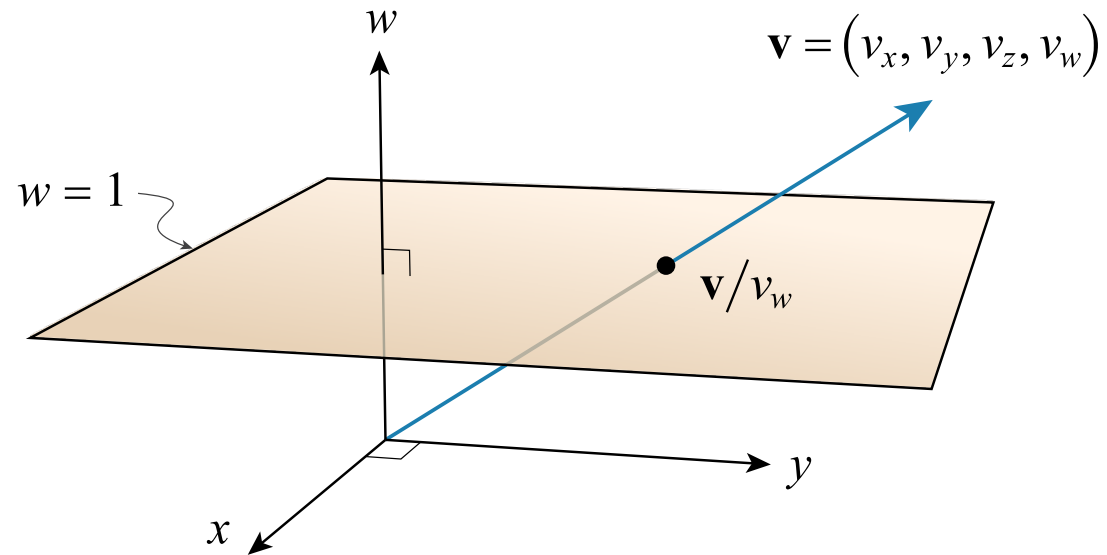
Normal Vector Transformation

- Normals don't transform like ordinary vectors
- That's because they're something else called *bivectors*



Homogeneous Coordinates

- 3D points are projections of 4D vectors



Homogeneous Coordinates

- Allows translations to be added to linear transformations

$$\begin{bmatrix} m_{11} & m_{12} & m_{13} \\ m_{21} & m_{22} & m_{23} \\ m_{31} & m_{32} & m_{33} \end{bmatrix} \begin{bmatrix} v_x \\ v_y \\ v_z \end{bmatrix}$$

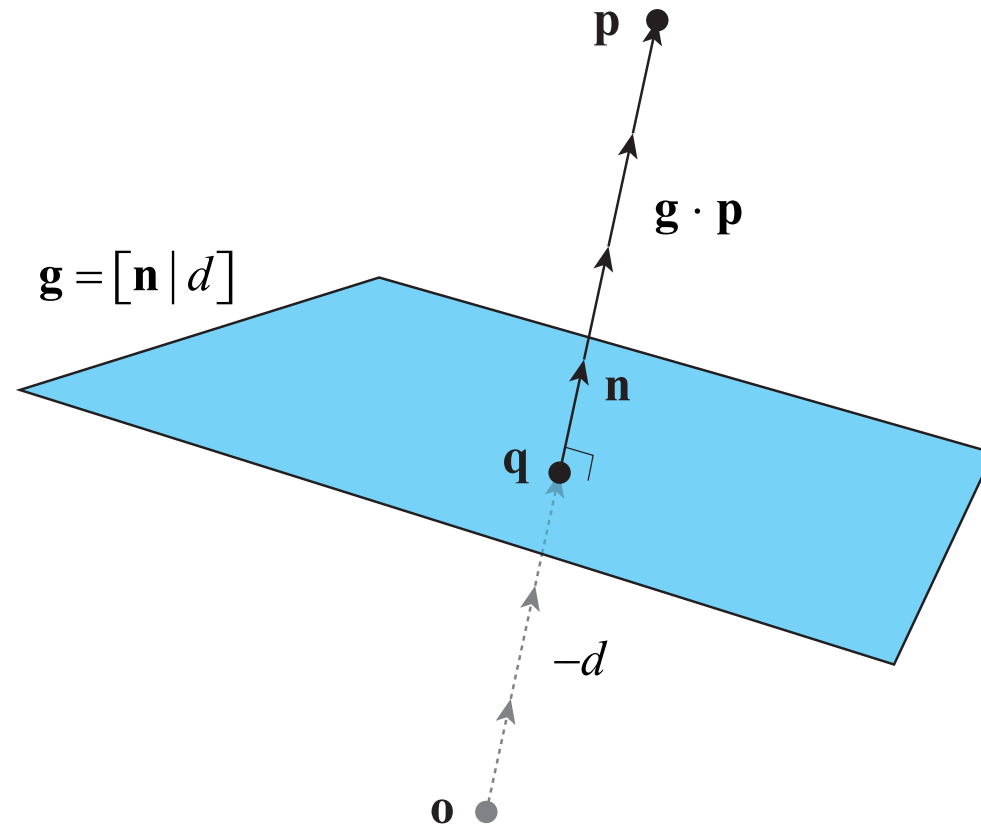
$$\begin{bmatrix} m_{11} & m_{12} & m_{13} & t_x \\ m_{21} & m_{22} & m_{23} & t_y \\ m_{31} & m_{32} & m_{33} & t_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} p_x \\ p_y \\ p_z \\ 1 \end{bmatrix}$$

Planes

- 4D dot product with point \mathbf{p} gives signed distance to plane \mathbf{g}

$$\mathbf{p} = (x, y, z, w)$$

$$\mathbf{g} = (n_x, n_y, n_z, d)$$



Plücker Coordinates

- Implicit representation of a line in 3D space
- Has 6 coordinates, 3 for direction \mathbf{v} and 3 for moment \mathbf{m}
- Given homogeneous points \mathbf{p} and \mathbf{q} on the line,

$$\mathbf{v} = p_w \mathbf{q}_{xyz} - q_w \mathbf{p}_{xyz}$$

$$\mathbf{m} = \mathbf{p}_{xyz} \times \mathbf{q}_{xyz}$$

- Same results for any two points spaced same distance apart
- Information about specific points is eliminated

Points, Lines, Planes

- Lots of formulas for combining geometries
- Discovered without knowledge of bigger picture
- We can better explain where all of these formulas come from

	Formula	Description
A	$\{w_1\mathbf{p}_2 - w_2\mathbf{p}_1 \mid \mathbf{p}_1 \times \mathbf{p}_2\}$	Line through two homogeneous points $(\mathbf{p}_1 \mid w_1)$ and $(\mathbf{p}_2 \mid w_2)$.
B	$\{\mathbf{p}_2 - \mathbf{p}_1 \mid \mathbf{p}_1 \times \mathbf{p}_2\}$	Line through two points \mathbf{p}_1 and \mathbf{p}_2 .
C	$\{\mathbf{v} \mid \mathbf{p} \times \mathbf{v}\}$	Line through point \mathbf{p} with direction \mathbf{v} .
D	$\{\mathbf{p} \mid \mathbf{0}\}$	Line through point \mathbf{p} and the origin.
E	$[\mathbf{v} \times \mathbf{p} + w\mathbf{m} \mid -\mathbf{p} \cdot \mathbf{m}]$	Plane containing line $\{\mathbf{v} \mid \mathbf{m}\}$ and homogeneous point $(\mathbf{p} \mid w)$.
F	$[\mathbf{v} \times \mathbf{p} + \mathbf{m} \mid -\mathbf{p} \cdot \mathbf{m}]$	Plane containing line $\{\mathbf{v} \mid \mathbf{m}\}$ and point \mathbf{p} .
G	$[\mathbf{v} \times \mathbf{u} \mid -\mathbf{u} \cdot \mathbf{m}]$	Plane containing line $\{\mathbf{v} \mid \mathbf{m}\}$, parallel to direction \mathbf{u} .
H	$[\mathbf{m} \mid \mathbf{0}]$	Plane containing line $\{\mathbf{v} \mid \mathbf{m}\}$ and the origin.
I	$\{\mathbf{n}_1 \times \mathbf{n}_2 \mid d_1\mathbf{n}_2 - d_2\mathbf{n}_1\}$	Line where two planes $[\mathbf{n}_1 \mid d_1]$ and $[\mathbf{n}_2 \mid d_2]$ intersect.
J	$(\mathbf{m} \times \mathbf{n} + d\mathbf{v} \mid -\mathbf{n} \cdot \mathbf{v})$	Homogeneous point where line $\{\mathbf{v} \mid \mathbf{m}\}$ intersects plane $[\mathbf{n} \mid d]$.
K	$\{w\mathbf{n} \mid \mathbf{p} \times \mathbf{n}\}$	Line through homogeneous point $(\mathbf{p} \mid w)$, perpendicular to plane $[\mathbf{n} \mid d]$.
L	$[\mathbf{v} \times \mathbf{n} \mid -\mathbf{n} \cdot \mathbf{m}]$	Plane containing line $\{\mathbf{v} \mid \mathbf{m}\}$, perpendicular to plane $[\mathbf{n} \mid d]$.
M	$[w\mathbf{v} \mid -\mathbf{p} \cdot \mathbf{v}]$	Plane containing homogeneous point $(\mathbf{p} \mid w)$, perpendicular to line $\{\mathbf{v} \mid \mathbf{m}\}$.
N	$(\mathbf{v} \times \mathbf{m} \mid \mathbf{v}^2)$	Homogeneous point closest to the origin on line $\{\mathbf{v} \mid \mathbf{m}\}$.
O	$(-d\mathbf{n} \mid \mathbf{n}^2)$	Homogeneous point closest to the origin on plane $[\mathbf{n} \mid d]$.
P	$[\mathbf{m} \times \mathbf{v} \mid \mathbf{m}^2]$	Plane farthest from the origin containing line $\{\mathbf{v} \mid \mathbf{m}\}$.
Q	$[-w\mathbf{p} \mid \mathbf{p}^2]$	Plane farthest from the origin containing point $(\mathbf{p} \mid w)$.
R	$\frac{\ w_1\mathbf{p}_2 - w_2\mathbf{p}_1\ }{ w_1w_2 }$	Distance between two homogeneous points $(\mathbf{p}_1 \mid w_1)$ and $(\mathbf{p}_2 \mid w_2)$.
S	$\frac{ \mathbf{v}_1 \cdot \mathbf{m}_2 + \mathbf{v}_2 \cdot \mathbf{m}_1 }{\ \mathbf{v}_1 \times \mathbf{v}_2\ }$	Distance between two lines $\{\mathbf{v}_1 \mid \mathbf{m}_1\}$ and $\{\mathbf{v}_2 \mid \mathbf{m}_2\}$.
T	$\frac{\ \mathbf{v} \times \mathbf{p} + \mathbf{m}\ }{\ \mathbf{v}\ }$	Distance from line $\{\mathbf{v} \mid \mathbf{m}\}$ to point \mathbf{p} .
U	$\frac{\ \mathbf{m}\ }{\ \mathbf{v}\ }$	Distance from line $\{\mathbf{v} \mid \mathbf{m}\}$ to the origin.
V	$\frac{ \mathbf{n} \cdot \mathbf{p} + d }{\ \mathbf{n}\ }$	Distance from plane $[\mathbf{n} \mid d]$ to point \mathbf{p} .
W	$\frac{ d }{\ \mathbf{n}\ }$	Distance from plane $[\mathbf{n} \mid d]$ to the origin.

Quaternions

- A quaternion \mathbf{q} represents a rotation in 3D space

$$\mathbf{q} = xi + yj + zk + w$$

$$i^2 = j^2 = k^2 = -1$$

$$ij = -ji = k$$

$$jk = -kj = i$$

$$ki = -ik = j$$

- Rotation through angle ϕ about axis \mathbf{a} is

$$\mathbf{q} = \left(\sin \frac{\phi}{2} \right) \mathbf{a} + \cos \frac{\phi}{2}$$

Quaternions

- A quaternion rotates a vector \mathbf{v} with the sandwich product

$$\mathbf{v}' = \mathbf{q}\mathbf{v}\mathbf{q}^* \qquad \mathbf{v} = v_x i + v_y j + v_z k$$

- \mathbf{q}^* is the conjugate of the quaternion:

$$\mathbf{q}^* = -xi - yj - zk + w$$

All Part of Same Algebraic Structure

- Non-vector result of cross product
- 4D homogeneous coordinates for points
- 6D Plücker coordinates for lines
- 4D plane representations
- Quaternions

4D Associative Projective Algebras

- 4D rigid exterior algebra
 - Homogeneous representation of 3D geometry
 - Points, lines, planes
 - Join, meet, projection, norm, distance, angle
- 4D rigid geometric algebra
 - Euclidean isometries in 3D space
 - Rotations, translations, screw transformations
 - Parameterization, interpolation

Exterior / Grassmann Algebra

- Wedge product \wedge
 - Combines dimensions of operands
 - Vectors square to zero:

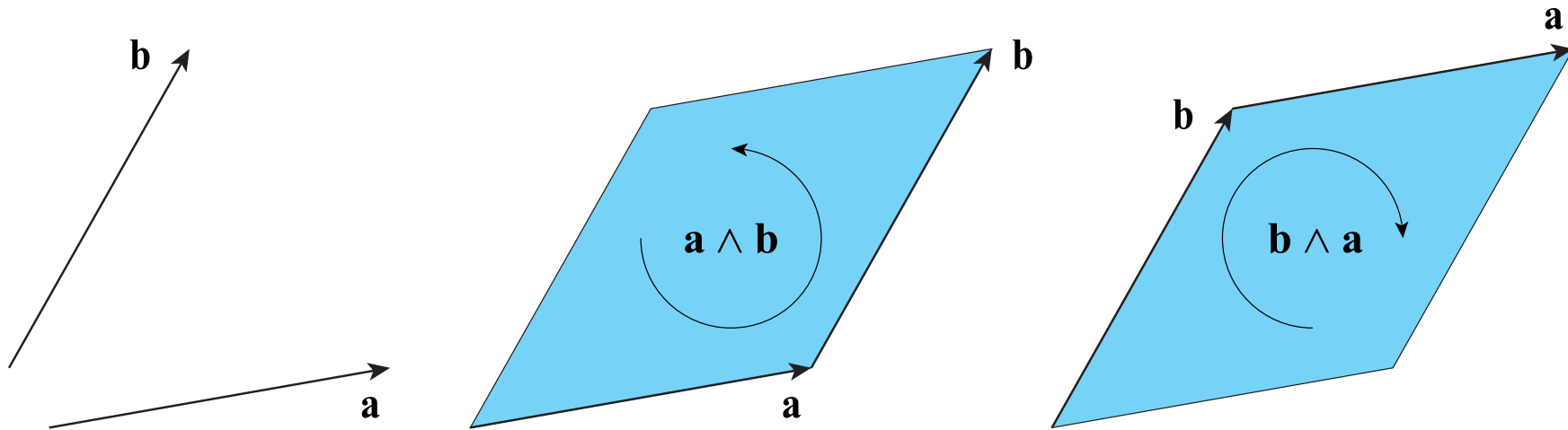
$$\mathbf{v} \wedge \mathbf{v} = 0$$

- Antisymmetric on vectors:

$$\mathbf{a} \wedge \mathbf{b} = -\mathbf{b} \wedge \mathbf{a}$$

Bivectors

- Wedge product of two vectors **a** and **b**
- Produces a new type of object



Bivectors

- Wedge product of two vectors **a** and **b**:

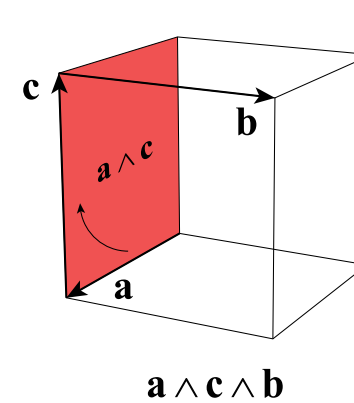
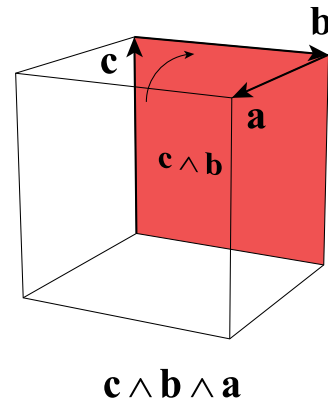
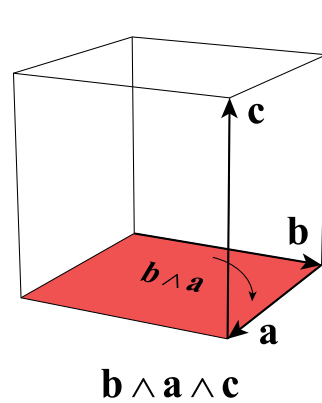
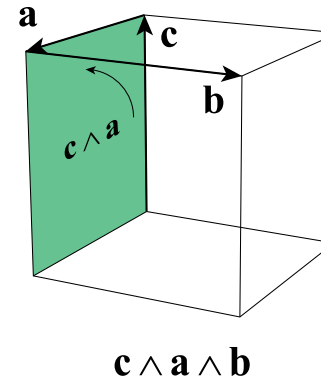
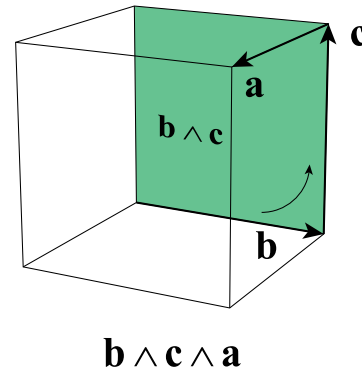
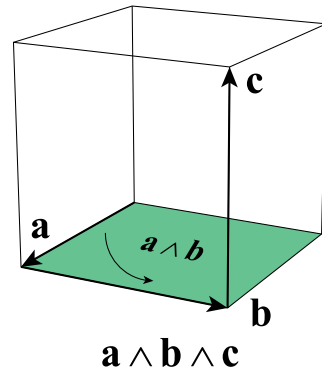
$$\begin{aligned}\mathbf{a} \wedge \mathbf{b} &= (a_y b_z - a_z b_y)(\mathbf{e}_2 \wedge \mathbf{e}_3) \\ &\quad + (a_z b_x - a_x b_z)(\mathbf{e}_3 \wedge \mathbf{e}_1) \\ &\quad + (a_x b_y - a_y b_x)(\mathbf{e}_1 \wedge \mathbf{e}_2)\end{aligned}$$

$$\begin{aligned}\mathbf{a} \wedge \mathbf{b} &= (a_y b_z - a_z b_y)\mathbf{e}_{23} \\ &\quad + (a_z b_x - a_x b_z)\mathbf{e}_{31} \\ &\quad + (a_x b_y - a_y b_x)\mathbf{e}_{12}\end{aligned}$$

- Cross product appears!

Trivectors

- Wedge product of three vectors **a**, **b**, and **c**



Trivectors

- Wedge product of three vectors **a**, **b**, and **c**

$$\mathbf{a} \wedge \mathbf{b} \wedge \mathbf{c} = (a_x b_y c_z + a_y b_z c_x + a_z b_x c_y - a_x b_z c_y - a_y b_x c_z - a_z b_y c_x) \mathbf{e}_{123}$$

- Determinant of 3×3 matrix with columns **a**, **b**, and **c**

Trivectors

- Wedge product of vector **a** and bivector **b**

$$\mathbf{a} = a_x \mathbf{e}_1 + a_y \mathbf{e}_2 + a_z \mathbf{e}_3$$

$$\mathbf{b} = b_x \mathbf{e}_{23} + b_y \mathbf{e}_{31} + b_z \mathbf{e}_{12}$$

$$\mathbf{a} \wedge \mathbf{b} = (a_x b_x + a_y b_y + a_z b_z) \mathbf{e}_{123}$$

- Dot product appears!

3D Vector Space

Scalars

s

Magnitudes

Vectors

$x\mathbf{e}_1 + y\mathbf{e}_2 + z\mathbf{e}_3$

Directed lengths

3D Exterior Algebra

Scalars

$$s\mathbf{1}$$

Magnitudes

Vectors

$$x\mathbf{e}_1 + y\mathbf{e}_2 + z\mathbf{e}_3$$

Directed lengths

Bivectors

$$x\mathbf{e}_{23} + y\mathbf{e}_{31} + z\mathbf{e}_{12}$$

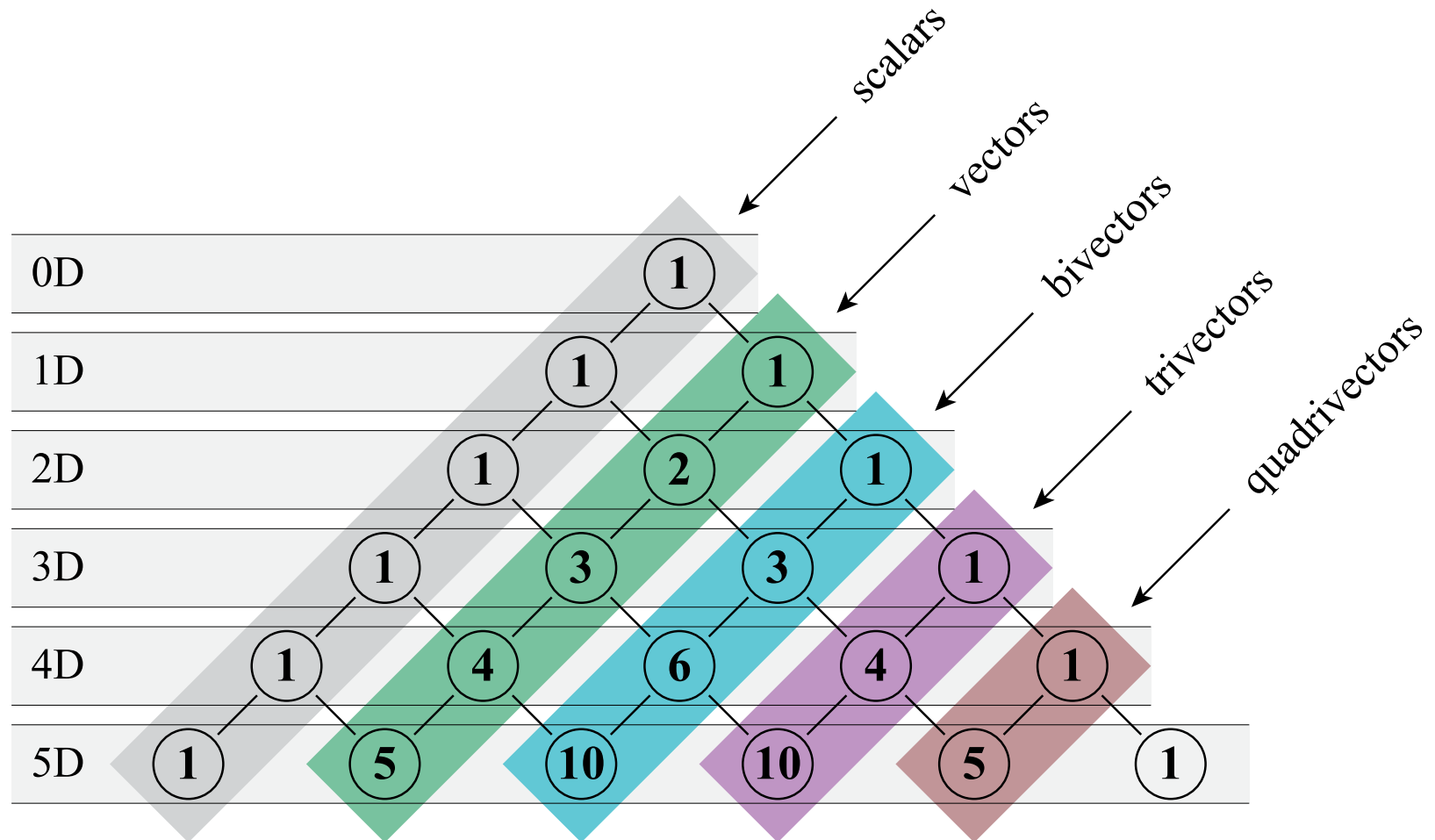
Directed areas

Trivectors

$$t\mathbf{e}_{123}$$

Directed volumes

Pascal's Triangle



Rigid Exterior / Geometric Algebra

- Projective algebra with one extra dimension
- Contains points, lines, planes in 3D
- Can perform rotations, translations, screw transformations

4D Exterior Algebra

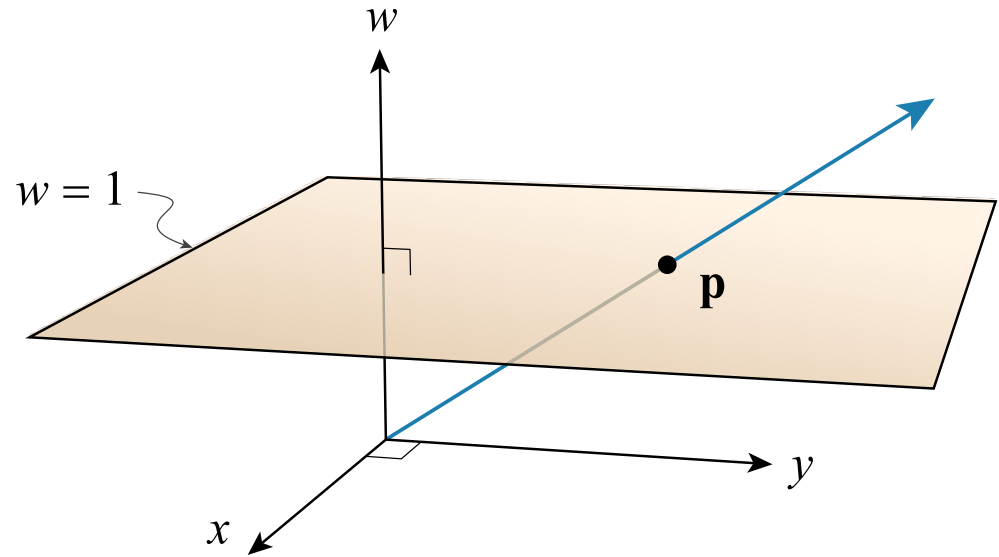
- Extends 4D vector space
- One scalar 1
- Four vector basis elements
- Six bivector basis elements
- Four trivector basis elements
- One antiscalar $\mathbb{1}$

Type	Values	Grade / Antigrade	
Scalar	1	0 / 4	<input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/>
Vectors	e_1 e_2 e_3 $e_4 = e_n$	1 / 3	<input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/>
Bivectors	$e_{41} = e_4 \wedge e_1$ $e_{42} = e_4 \wedge e_2$ $e_{43} = e_4 \wedge e_3$ $e_{23} = e_2 \wedge e_3$ $e_{31} = e_3 \wedge e_1$ $e_{12} = e_1 \wedge e_2$	2 / 2	<input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/>
Trivectors / Antivectors	$e_{423} = e_4 \wedge e_2 \wedge e_3$ $e_{431} = e_4 \wedge e_3 \wedge e_1$ $e_{412} = e_4 \wedge e_1 \wedge e_2$ $e_{321} = e_3 \wedge e_2 \wedge e_1$	3 / 1	<input type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/>
Antiscalar	$\mathbb{1} = e_1 \wedge e_2 \wedge e_3 \wedge e_4$	4 / 0	<input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/>

Point

$$\mathbf{p} = p_x \mathbf{e}_1 + p_y \mathbf{e}_2 + p_z \mathbf{e}_3 + p_w \mathbf{e}_4$$

Position Weight



Special Points

- The origin is simply the point e_4
- Point with zero weight lies at infinity in (x, y, z) direction
- Points at infinity in opposite directions are equivalent

Line

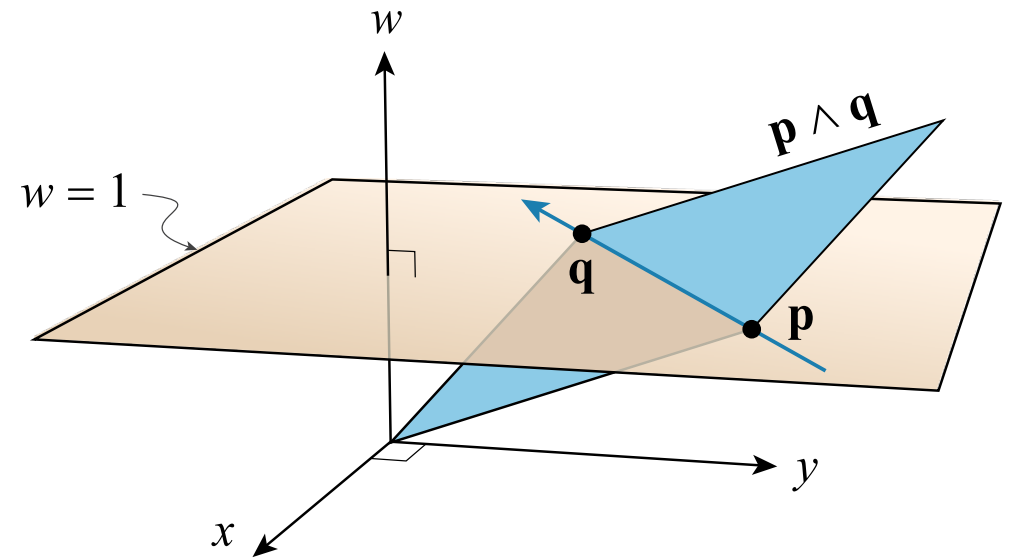
$$\mathbf{p} \wedge \mathbf{q} = (q_x p_w - p_x q_w) \mathbf{e}_{41} + (q_y p_w - p_y q_w) \mathbf{e}_{42} + (q_z p_w - p_z q_w) \mathbf{e}_{43} \\ + (p_y q_z - p_z q_y) \mathbf{e}_{23} + (p_z q_x - p_x q_z) \mathbf{e}_{31} + (p_x q_y - p_y q_x) \mathbf{e}_{12}$$

$$\mathbf{l} = l_{vx} \mathbf{e}_{41} + l_{vy} \mathbf{e}_{42} + l_{vz} \mathbf{e}_{43} + l_{mx} \mathbf{e}_{23} + l_{my} \mathbf{e}_{31} + l_{mz} \mathbf{e}_{12}$$

Direction

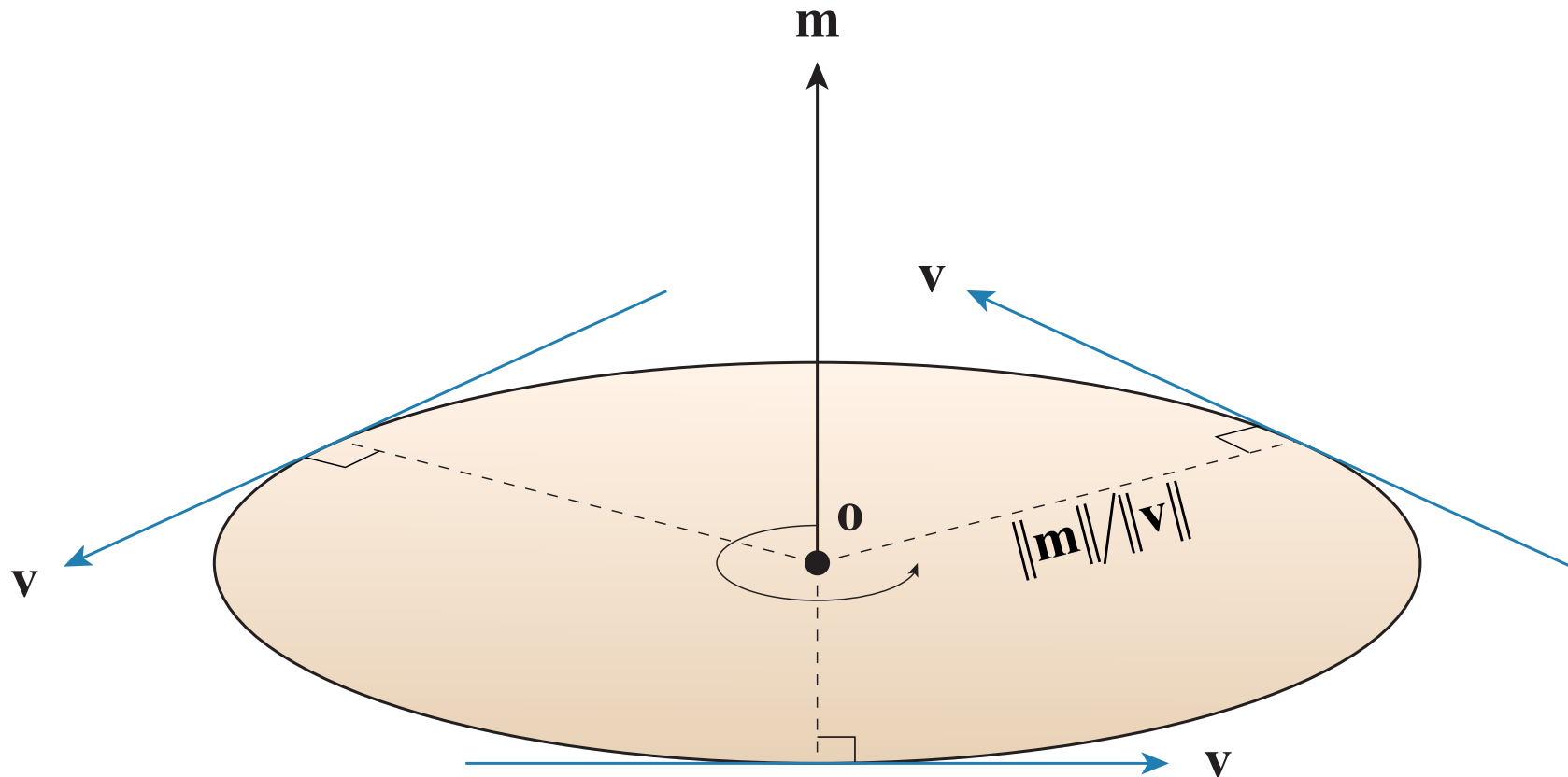
Moment

$$\mathbf{l}_v \cdot \mathbf{l}_m = 0$$



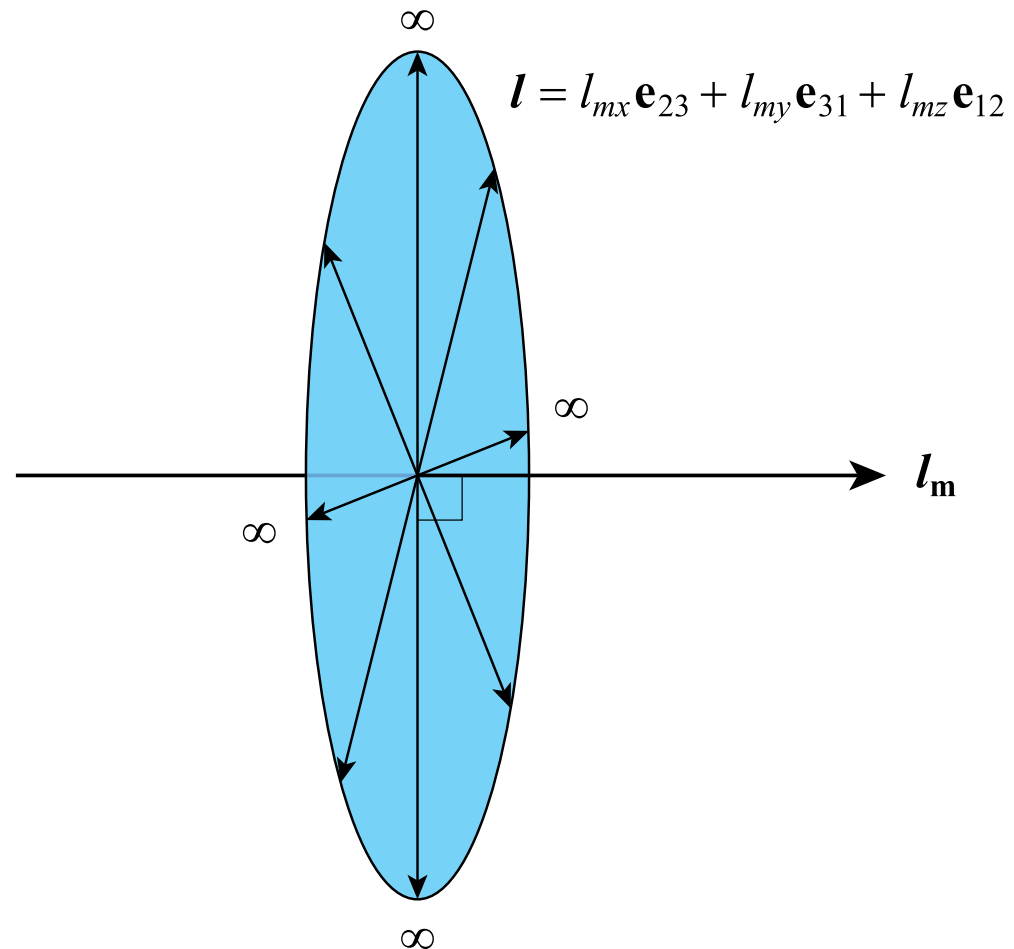
Line Moment

- Contains position information



Lines at Infinity

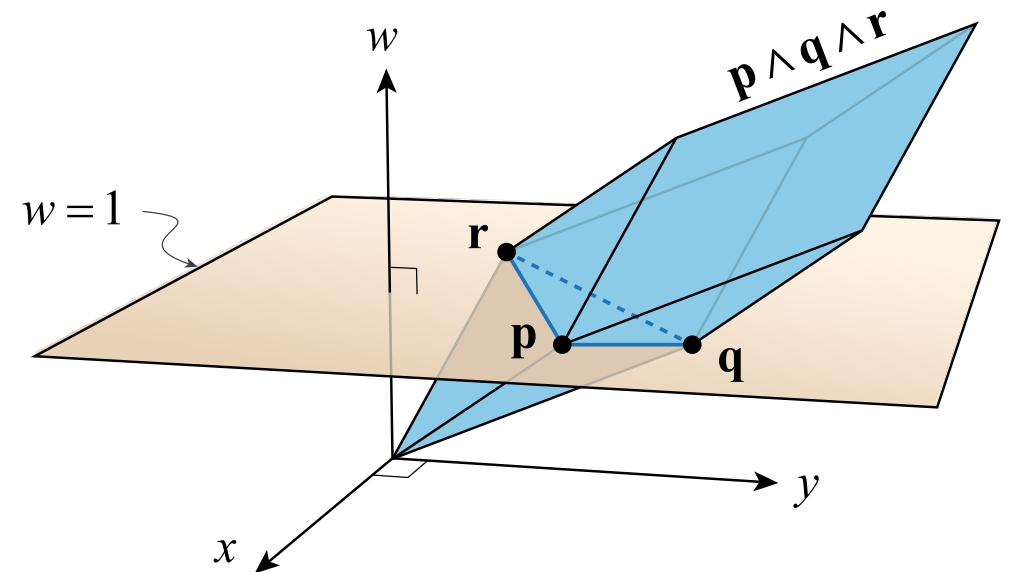
- Line with zero direction lies at infinity



Plane

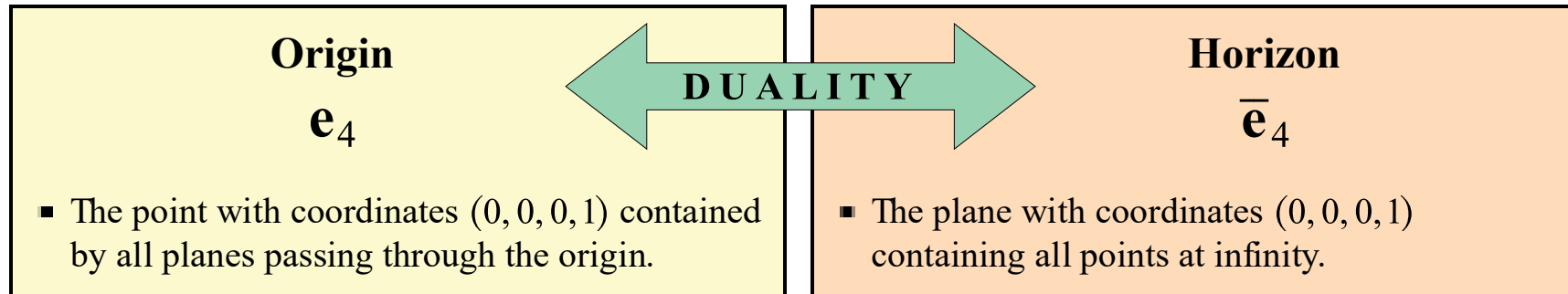
$$\begin{aligned} \mathbf{l} \wedge \mathbf{p} = & (l_{vy}p_z - l_{vz}p_y + l_{mx})\mathbf{e}_{423} + (l_{vz}p_x - l_{vx}p_z + l_{my})\mathbf{e}_{431} \\ & + (l_{vx}p_y - l_{vy}p_x + l_{mz})\mathbf{e}_{412} - (l_{mx}p_x + l_{my}p_y + l_{mz}p_z)\mathbf{e}_{321} \end{aligned}$$

$$\mathbf{g} = \underbrace{g_x \mathbf{e}_{423} + g_y \mathbf{e}_{431} + g_z \mathbf{e}_{412}}_{\text{Normal}} + \underbrace{g_w \mathbf{e}_{321}}_{\text{Position}}$$



Horizon

- Plane with zero normal lies at infinity: $g_w \mathbf{e}_{321}$
- Contains all points at infinity, all lines at infinity
- Given special name *horizon*



4D Exterior Algebra

Scalars

$$s\mathbf{1}$$

Magnitudes

Vectors

$$x\mathbf{e}_1 + y\mathbf{e}_2 + z\mathbf{e}_3 + w\mathbf{e}_4$$

Points

Bivectors

$$v_x\mathbf{e}_{41} + v_y\mathbf{e}_{42} + v_z\mathbf{e}_{43} + m_x\mathbf{e}_{23} + m_y\mathbf{e}_{31} + m_z\mathbf{e}_{12}$$

Lines

Trivectors

$$g_x\mathbf{e}_{423} + g_y\mathbf{e}_{431} + g_z\mathbf{e}_{412} + g_w\mathbf{e}_{321}$$

Planes

Quadrivectors

$$t\mathbf{1}$$

Magnitudes

Complements

- Complement inverts full / empty dimensions
- Right complement denoted by overbar
- Left complement denoted by underbar
- For basis element \mathbf{u} ,

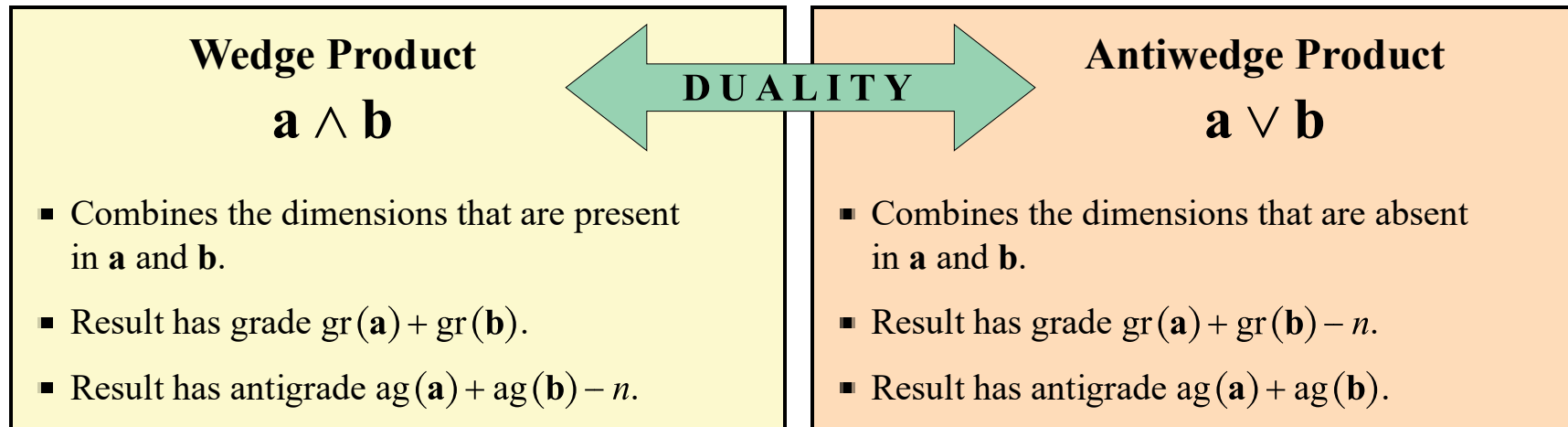
$$\mathbf{u} \wedge \bar{\mathbf{u}} = \mathbb{1}$$

$$\underline{\mathbf{u}} \wedge \mathbf{u} = \mathbb{1}$$

\mathbf{u}	$\mathbb{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$
$\bar{\mathbf{u}}$	$\mathbb{1}$	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$-\mathbf{e}_{23}$	$-\mathbf{e}_{31}$	$-\mathbf{e}_{12}$	$-\mathbf{e}_{41}$	$-\mathbf{e}_{42}$	$-\mathbf{e}_{43}$	$-\mathbf{e}_1$	$-\mathbf{e}_2$	$-\mathbf{e}_3$	$-\mathbf{e}_4$	$\mathbb{1}$
$\underline{\mathbf{u}}$	$\mathbb{1}$	$-\mathbf{e}_{423}$	$-\mathbf{e}_{431}$	$-\mathbf{e}_{412}$	$-\mathbf{e}_{321}$	$-\mathbf{e}_{23}$	$-\mathbf{e}_{31}$	$-\mathbf{e}_{12}$	$-\mathbf{e}_{41}$	$-\mathbf{e}_{42}$	$-\mathbf{e}_{43}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	$\mathbb{1}$

Antiwedge Product

- Antiwedge product denoted by \vee



De Morgan Laws

- Every operation with 'anti' in its name satisfies a De Morgan law:

$$\overline{\mathbf{a} \vee \mathbf{b}} = \bar{\mathbf{a}} \wedge \bar{\mathbf{b}}$$

$$\underline{\mathbf{a} \wedge \mathbf{b}} = \underline{\mathbf{a}} \vee \underline{\mathbf{b}}$$

- To calculate anti-operation,
 - Take a complement of each input
 - Perform the regular operation
 - Take opposite complement of the result

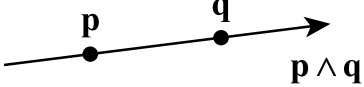
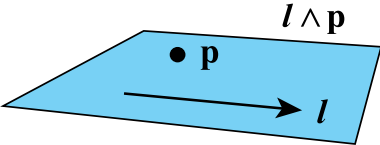
4D Exterior Antiproduct

Antiwedge Product $\mathbf{a} \vee \mathbf{b}$

$\mathbf{a} \backslash \mathbf{b}$	$\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$
$\mathbf{1}$	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$\mathbf{1}$
\mathbf{e}_1	0	0	0	0	0	0	0	0	0	0	0	$\mathbf{1}$	0	0	0	\mathbf{e}_1
\mathbf{e}_2	0	0	0	0	0	0	0	0	0	0	0	0	$\mathbf{1}$	0	0	\mathbf{e}_2
\mathbf{e}_3	0	0	0	0	0	0	0	0	0	0	0	0	0	$\mathbf{1}$	0	\mathbf{e}_3
\mathbf{e}_4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	$\mathbf{1}$	\mathbf{e}_4
\mathbf{e}_{41}	0	0	0	0	0	0	0	0	$-\mathbf{1}$	0	0	$-\mathbf{e}_4$	0	0	\mathbf{e}_1	\mathbf{e}_{41}
\mathbf{e}_{42}	0	0	0	0	0	0	0	0	0	$-\mathbf{1}$	0	0	$-\mathbf{e}_4$	0	\mathbf{e}_2	\mathbf{e}_{42}
\mathbf{e}_{43}	0	0	0	0	0	0	0	0	0	0	$-\mathbf{1}$	0	0	$-\mathbf{e}_4$	\mathbf{e}_3	\mathbf{e}_{43}
\mathbf{e}_{23}	0	0	0	0	0	$-\mathbf{1}$	0	0	0	0	0	0	\mathbf{e}_3	$-\mathbf{e}_2$	0	\mathbf{e}_{23}
\mathbf{e}_{31}	0	0	0	0	0	0	$-\mathbf{1}$	0	0	0	0	$-\mathbf{e}_3$	0	\mathbf{e}_1	0	\mathbf{e}_{31}
\mathbf{e}_{12}	0	0	0	0	0	0	0	$-\mathbf{1}$	0	0	0	\mathbf{e}_2	$-\mathbf{e}_1$	0	0	\mathbf{e}_{12}
\mathbf{e}_{423}	0	$-\mathbf{1}$	0	0	0	$-\mathbf{e}_4$	0	0	0	$-\mathbf{e}_3$	\mathbf{e}_2	0	$-\mathbf{e}_{43}$	\mathbf{e}_{42}	\mathbf{e}_{23}	\mathbf{e}_{423}
\mathbf{e}_{431}	0	0	$-\mathbf{1}$	0	0	0	$-\mathbf{e}_4$	0	\mathbf{e}_3	0	$-\mathbf{e}_1$	\mathbf{e}_{43}	0	$-\mathbf{e}_{41}$	\mathbf{e}_{31}	\mathbf{e}_{431}
\mathbf{e}_{412}	0	0	0	$-\mathbf{1}$	0	0	0	$-\mathbf{e}_4$	$-\mathbf{e}_2$	\mathbf{e}_1	0	$-\mathbf{e}_{42}$	\mathbf{e}_{41}	0	\mathbf{e}_{12}	\mathbf{e}_{412}
\mathbf{e}_{321}	0	0	0	0	$-\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	0	0	0	$-\mathbf{e}_{23}$	$-\mathbf{e}_{31}$	$-\mathbf{e}_{12}$	0	\mathbf{e}_{321}
$\mathbb{1}$	$\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$

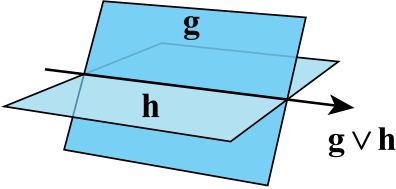
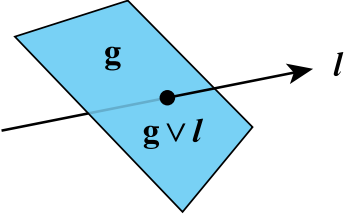
Join

- Wedge product performs join operation
- Produces higher-dimensional object containing both operands

Join Operation	Illustration
<p>Line containing points \mathbf{p} and \mathbf{q}.</p> $\mathbf{p} \wedge \mathbf{q} = (p_w q_x - p_x q_w) \mathbf{e}_{41} + (p_y q_z - p_z q_y) \mathbf{e}_{23}$ $+ (p_w q_y - p_y q_w) \mathbf{e}_{42} + (p_z q_x - p_x q_z) \mathbf{e}_{31}$ $+ (p_w q_z - p_z q_w) \mathbf{e}_{43} + (p_x q_y - p_y q_x) \mathbf{e}_{12}$	
<p>Plane containing line l and point \mathbf{p}.</p> $l \wedge \mathbf{p} = (l_{vy} p_z - l_{vz} p_y + l_{mx} p_w) \mathbf{e}_{423}$ $+ (l_{vz} p_x - l_{vx} p_z + l_{my} p_w) \mathbf{e}_{431}$ $+ (l_{vx} p_y - l_{vy} p_x + l_{mz} p_w) \mathbf{e}_{412}$ $- (l_{mx} p_x + l_{my} p_y + l_{mz} p_z) \mathbf{e}_{321}$	

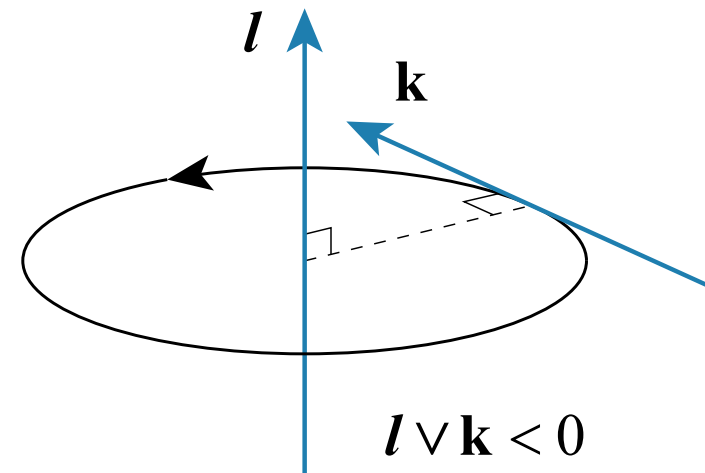
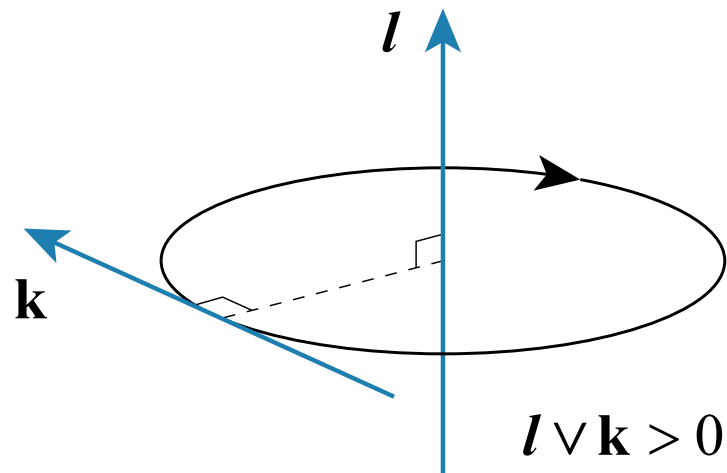
Meet

- Antiwedge product performs meet operation
- Produces lower-dimensional object at intersection of operands

Meet Operation	Illustration
<p>Line where planes g and h intersect.</p> $\mathbf{g} \vee \mathbf{h} = (g_z h_y - g_y h_z) \mathbf{e}_{41} + (g_x h_w - g_w h_x) \mathbf{e}_{23} \\ + (g_x h_z - g_z h_x) \mathbf{e}_{42} + (g_y h_w - g_w h_y) \mathbf{e}_{31} \\ + (g_y h_x - g_x h_y) \mathbf{e}_{43} + (g_z h_w - g_w h_z) \mathbf{e}_{12}$	 <p>The diagram shows two light blue planes, labeled 'g' and 'h', intersecting at a line. An arrow points from the intersection line to the label 'g ∨ h'.</p>
<p>Point where plane g and line l intersect.</p> $\mathbf{g} \vee \mathbf{l} = (g_z l_{my} - g_y l_{mz} + g_w l_{vx}) \mathbf{e}_1 \\ + (g_x l_{mz} - g_z l_{mx} + g_w l_{vy}) \mathbf{e}_2 \\ + (g_y l_{mx} - g_x l_{my} + g_w l_{vz}) \mathbf{e}_3 \\ - (g_x l_{vx} + g_y l_{vy} + g_z l_{vz}) \mathbf{e}_4$	 <p>The diagram shows a light blue plane labeled 'g' intersected by a line labeled 'l'. A black dot marks the intersection point, which is labeled 'g ∨ l'.</p>

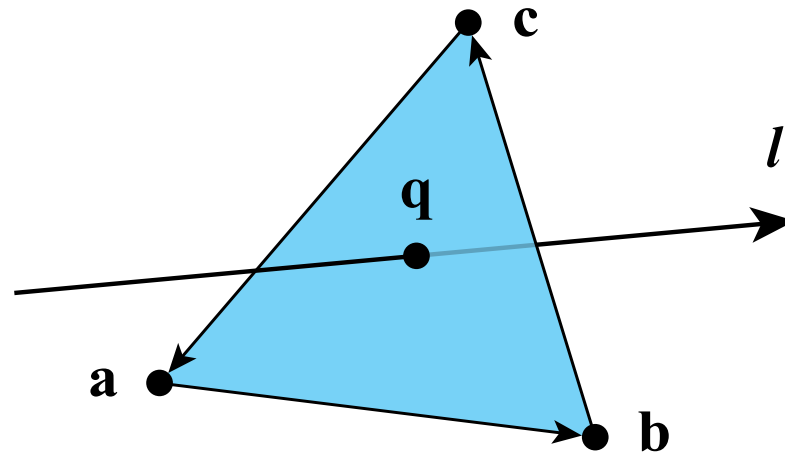
Line Crossing

- Sign of wedge product between lines gives crossing orientation



Line-Triangle Intersection

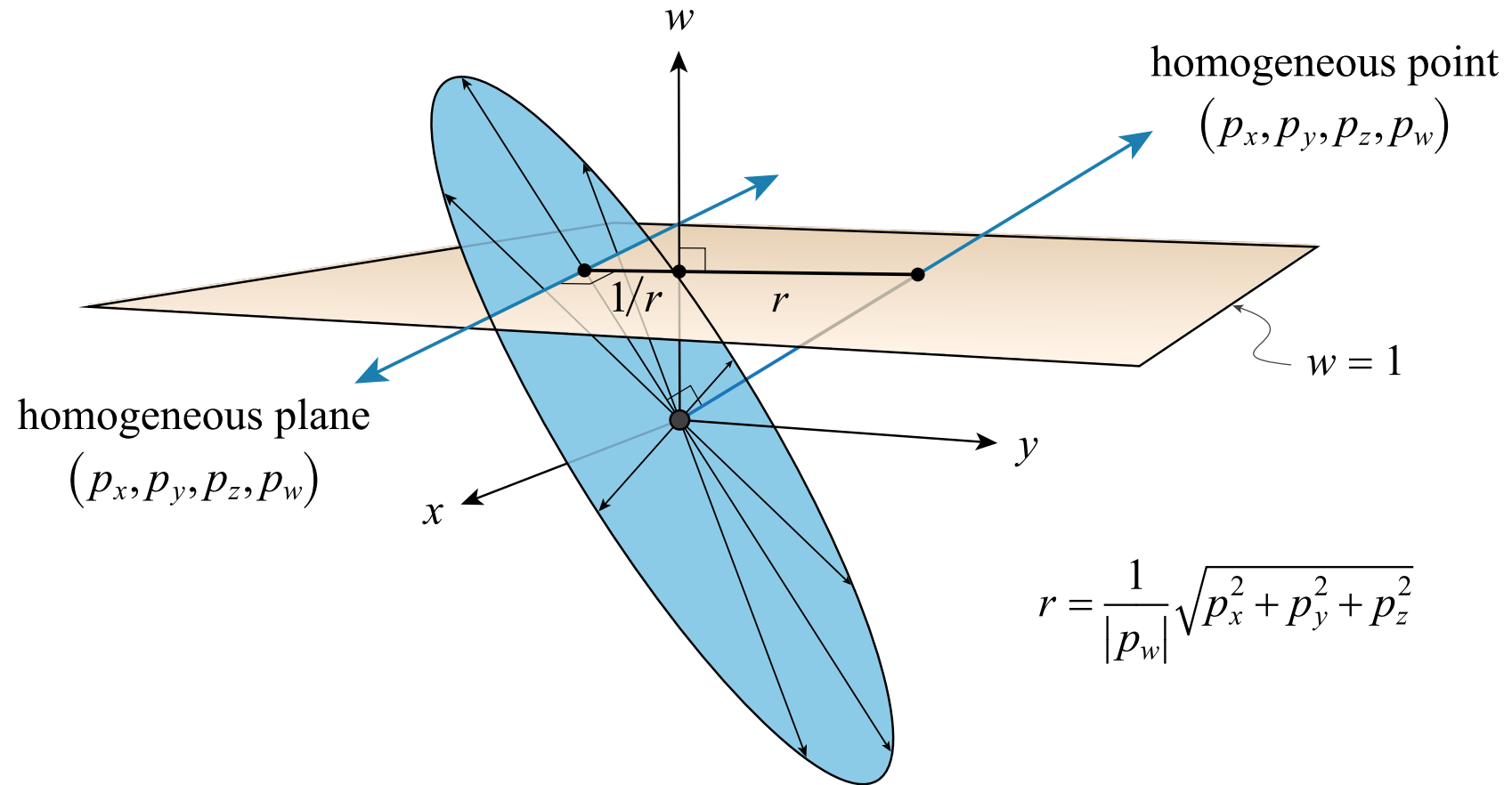
- Wedge product with all three edges of CCW-wound triangle must be positive



Duality

- Every object can be interpreted as two different things
- Every operation performs two different actions
- One interpretation corresponds to regular space
- The other interpretation corresponds to *antispaces*

Duality



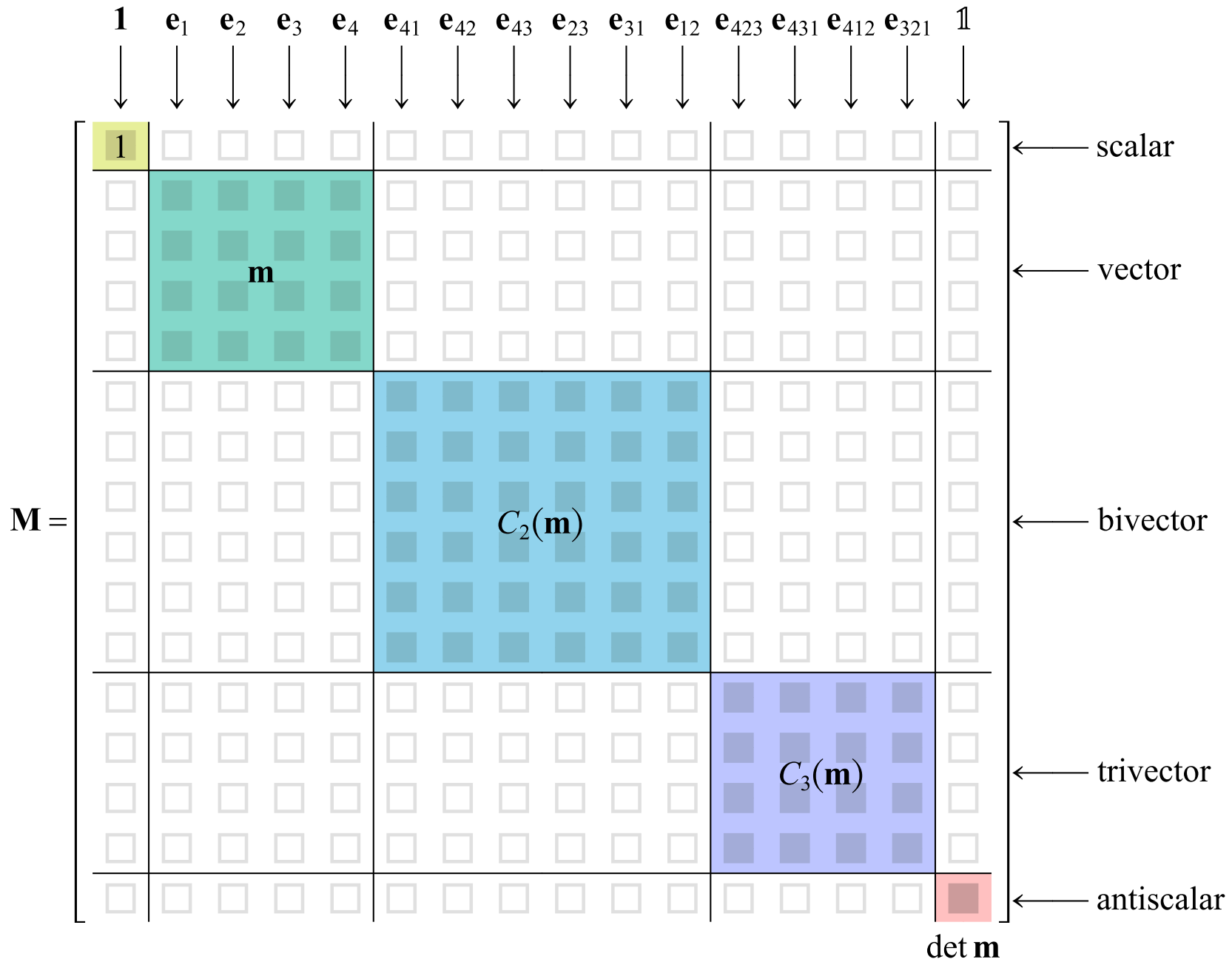
Exomorphisms

- Given an $n \times n$ linear transformation \mathbf{m} that operates on vectors
- The exomorphism \mathbf{M} is the $2^n \times 2^n$ matrix that operates on the whole algebra
- Exomorphism preserves structure under the wedge product:

$$\mathbf{M}(\mathbf{a} \wedge \mathbf{b}) = (\mathbf{M}\mathbf{a}) \wedge (\mathbf{M}\mathbf{b})$$

Exomorphisms

- Matrix \mathbf{M} is block diagonal
- Each block has columns given by wedge products of columns of the original matrix \mathbf{m}
- These are called *compound matrices* of \mathbf{m}



Translation Exomorphism

$$\mathbf{m} = \begin{bmatrix} 1 & 0 & 0 & t_x \\ 0 & 1 & 0 & t_y \\ 0 & 0 & 1 & t_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$C_2(\mathbf{m}) = \begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & -t_z & t_y & 1 & 0 & 0 \\ t_z & 0 & -t_x & 0 & 1 & 0 \\ -t_y & t_x & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$C_3(\mathbf{m}) = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ -t_x & -t_y & -t_z & 1 \end{bmatrix}$$

Nonuniform Scale Exomorphism

$$\mathbf{m} = \begin{bmatrix} s_x & 0 & 0 & 0 \\ 0 & s_y & 0 & 0 \\ 0 & 0 & s_z & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$C_2(\mathbf{m}) = \begin{bmatrix} s_x & 0 & 0 & 0 & 0 & 0 \\ 0 & s_y & 0 & 0 & 0 & 0 \\ 0 & 0 & s_z & 0 & 0 & 0 \\ 0 & 0 & 0 & s_y s_z & 0 & 0 \\ 0 & 0 & 0 & 0 & s_z s_x & 0 \\ 0 & 0 & 0 & 0 & 0 & s_x s_y \end{bmatrix}$$

$$C_3(\mathbf{m}) = \begin{bmatrix} s_y s_z & 0 & 0 & 0 \\ 0 & s_z s_x & 0 & 0 \\ 0 & 0 & s_x s_y & 0 \\ 0 & 0 & 0 & s_x s_y s_z \end{bmatrix}$$

The Metric Tensor

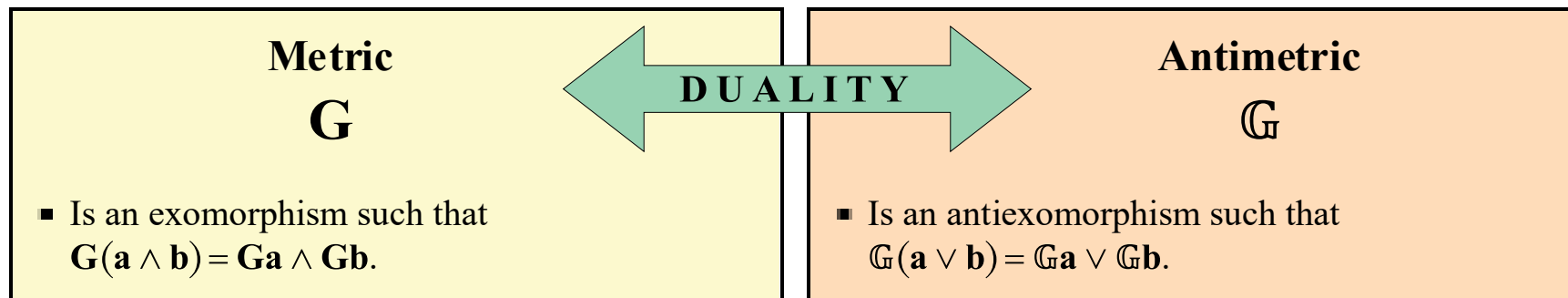
- $n \times n$ matrix that defines dot products of vectors

$$\mathbf{g} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{l} \mathbf{e}_1 \cdot \mathbf{e}_1 = +1 \\ \mathbf{e}_2 \cdot \mathbf{e}_2 = +1 \\ \mathbf{e}_3 \cdot \mathbf{e}_3 = +1 \\ \mathbf{e}_4 \cdot \mathbf{e}_4 = 0 \end{array}$$

$$\mathbf{g}_{ij} \equiv \mathbf{v}_i \cdot \mathbf{v}_j$$

Metric Exomorphism

- The metric tensor is a linear transformation
- It can be extended to a $2^n \times 2^n$ matrix \mathbf{G} that applies to entire exterior algebra
- There is also an *antimetric* that satisfies $\mathbb{G}\mathbf{u} = \underline{\mathbf{G}\bar{\mathbf{u}}} = \overline{\mathbf{G}\underline{\mathbf{u}}}$



Metric and Antimetric

$G =$

1																					
	1	0	0	0																	
	0	1	0	0																	
	0	0	1	0																	
	0	0	0	0																	
					0	0	0	0	0	0											
					0	0	0	0	0	0											
					0	0	0	0	0	0											
					0	0	0	1	0	0											
					0	0	0	0	1	0											
					0	0	0	0	0	1											
											0	0	0	0							
											0	0	0	0							
											0	0	0	0							
											0	0	0	1							
																			0		

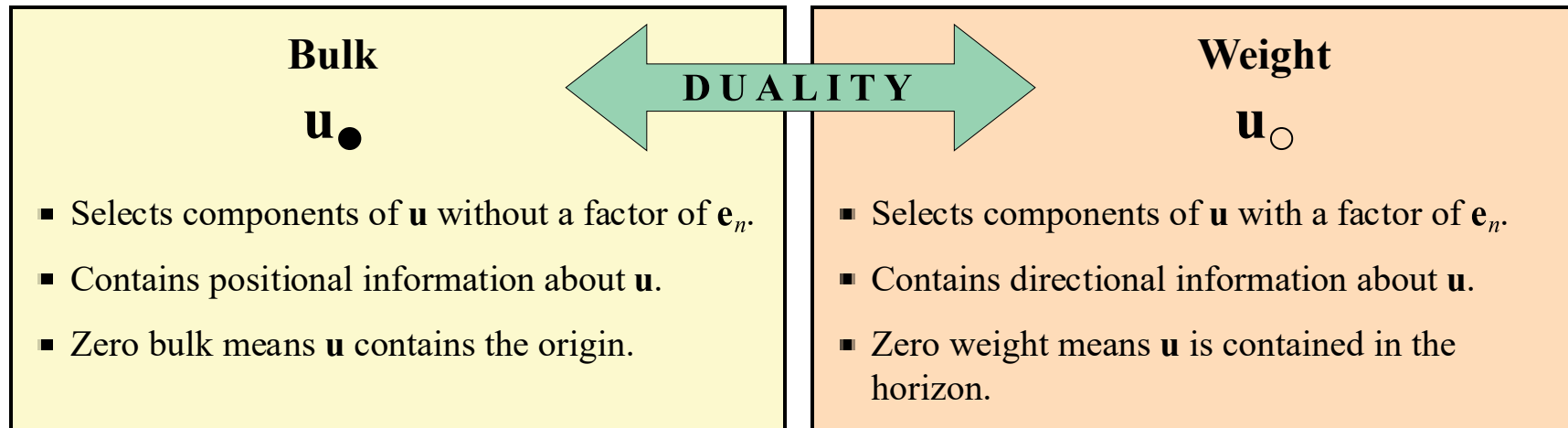
$G =$

0																					
	0	0	0	0																	
	0	0	0	0																	
	0	0	0	0																	
	0	0	0	1																	
					1	0	0	0	0	0											
					0	1	0	0	0	0											
					0	0	1	0	0	0											
					0	0	0	0	0	0											
					0	0	0	0	0	0											
					0	0	0	0	0	0											
															1	0	0	0			
															0	1	0	0			
															0	0	1	0			
															0	0	0	0			
																			1		

$$GG = \det(\mathbf{g})\mathbf{I}$$

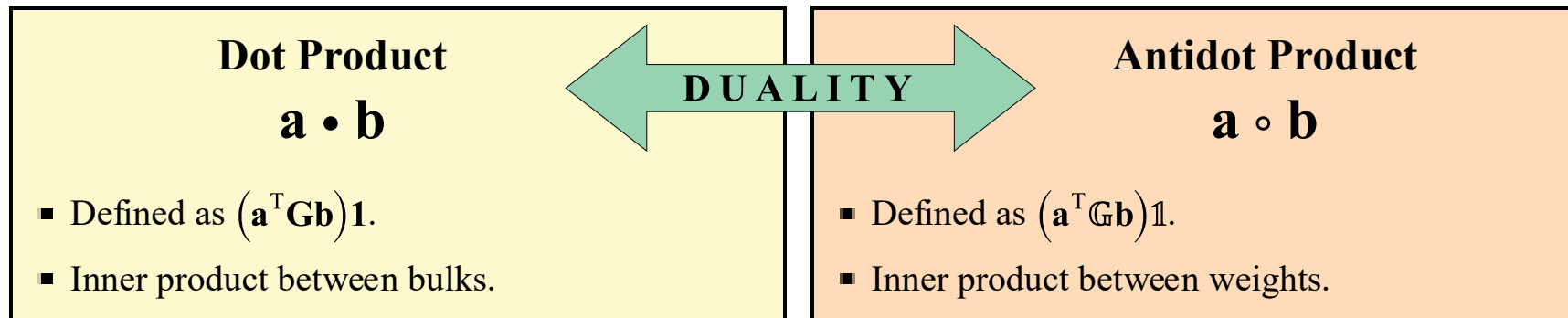
Bulk and Weight

- Bulk $\mathbf{u}_\bullet = \mathbb{G}\mathbf{u}$ All components without factor \mathbf{e}_4
- Weight $\mathbf{u}_\circ = \mathbb{G}\mathbf{u}$ All components with factor \mathbf{e}_4



Inner Products

- Dot product defined by metric: $\mathbf{a} \cdot \mathbf{b} = (\mathbf{a}^T \mathbf{G} \mathbf{b}) \mathbf{1}$
- Antidot product defined by antimetric: $\mathbf{a} \circ \mathbf{b} = (\mathbf{a}^T \mathbb{G} \mathbf{b}) \mathbf{1}$
- Satisfies De Morgan law: $\mathbf{a} \circ \mathbf{b} = \underline{\underline{\mathbf{a} \cdot \mathbf{b}}}$



Bulk and Weight Norms

- Two dot products induce two norms

- Bulk norm: $\|\mathbf{u}\|_{\bullet} = \sqrt{\mathbf{u} \cdot \mathbf{u}}$

- Weight norm: $\|\mathbf{u}\|_{\circ} = \sqrt{\mathbf{u} \circ \mathbf{u}}$

- Can generally have arbitrary values for same geometry due to homogeneity

Bulk and Weight Norms

Type	Bulk Norm	Weight Norm
Point \mathbf{p}	$\ \mathbf{p}\ _{\bullet} = \mathbf{1}\sqrt{p_x^2 + p_y^2 + p_z^2}$	$\ \mathbf{p}\ _{\circ} = p_w \mathbf{1}$
Line l	$\ l\ _{\bullet} = \mathbf{1}\sqrt{l_{mx}^2 + l_{my}^2 + l_{mz}^2}$	$\ l\ _{\circ} = \mathbf{1}\sqrt{l_{vx}^2 + l_{vy}^2 + l_{vz}^2}$
Plane \mathbf{g}	$\ \mathbf{g}\ _{\bullet} = g_w \mathbf{1}$	$\ \mathbf{g}\ _{\circ} = \mathbf{1}\sqrt{g_x^2 + g_y^2 + g_z^2}$

Unitization

- An object is *unitized* when its weight has magnitude one

Type	Definition	Unitization
Point \mathbf{p}	$\mathbf{p} = p_x \mathbf{e}_1 + p_y \mathbf{e}_2 + p_z \mathbf{e}_3 + p_w \mathbf{e}_4$	$p_w^2 = 1$
Line l	$l = l_{vx} \mathbf{e}_{41} + l_{vy} \mathbf{e}_{42} + l_{vz} \mathbf{e}_{43} + l_{mx} \mathbf{e}_{23} + l_{my} \mathbf{e}_{31} + l_{mz} \mathbf{e}_{12}$	$l_{vx}^2 + l_{vy}^2 + l_{vz}^2 = 1$
Plane \mathbf{g}	$\mathbf{g} = g_x \mathbf{e}_{423} + g_y \mathbf{e}_{431} + g_z \mathbf{e}_{412} + g_w \mathbf{e}_{321}$	$g_x^2 + g_y^2 + g_z^2 = 1$

Geometric Norm

- Bulk and weight norms by themselves not very meaningful
- But add them, and result is a *homogeneous magnitude*
- Represents distance from origin
- Called the *geometric norm*

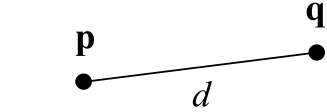
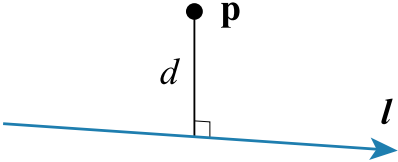
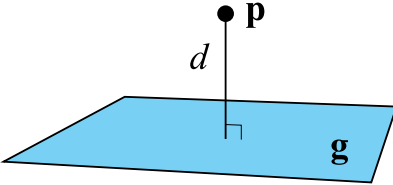
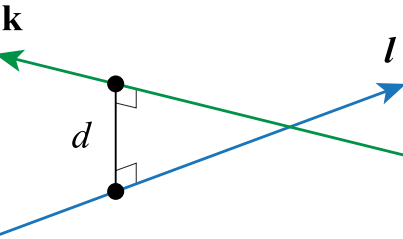
$$\|\mathbf{u}\| = \|\mathbf{u}\|_{\bullet} + \|\mathbf{u}\|_{\circ} = \sqrt{\mathbf{u} \cdot \mathbf{u}} + \sqrt{\mathbf{u} \circ \mathbf{u}}$$

- Two-component quantity, sum of scalar and antiscalar $s\mathbf{1} + t\mathbf{1}$
- Can be unitized by making weight one

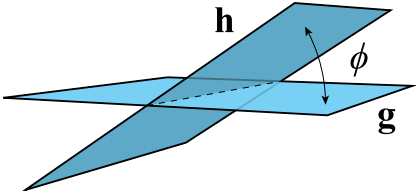
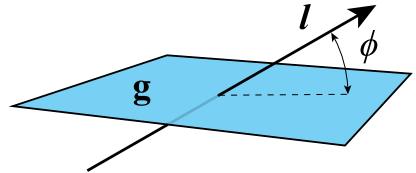
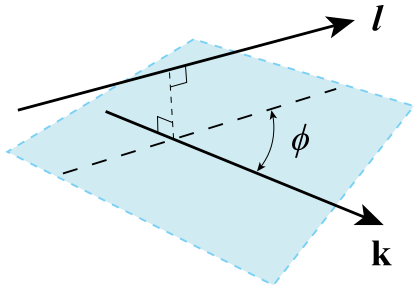
Geometric Norm

Type	Geometric Norm	Interpretation
Point \mathbf{p}	$\ \widehat{\mathbf{p}}\ = \frac{\sqrt{p_x^2 + p_y^2 + p_z^2}}{ p_w }$	Distance from the origin to the point \mathbf{p} .
Line l	$\ \widehat{l}\ = \frac{\sqrt{l_{mx}^2 + l_{my}^2 + l_{mz}^2}}{\sqrt{l_{vx}^2 + l_{vy}^2 + l_{vz}^2}}$	Perpendicular distance from the origin to the line l .
Plane \mathbf{g}	$\ \widehat{\mathbf{g}}\ = \frac{ g_w }{\sqrt{g_x^2 + g_y^2 + g_z^2}}$	Perpendicular distance from the origin to the plane \mathbf{g} .

Euclidean Distance

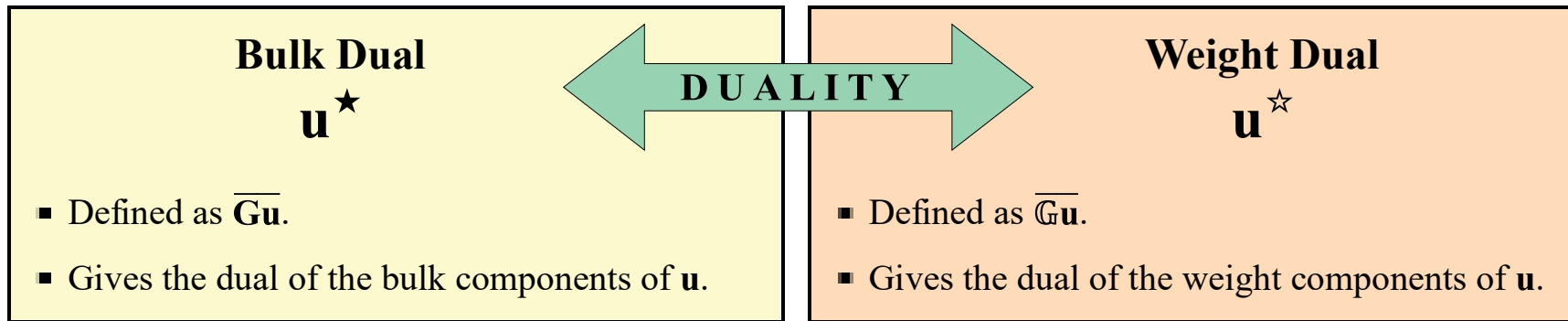
Distance Formula	Illustration
Distance d between points \mathbf{p} and \mathbf{q} . $d(\mathbf{p}, \mathbf{q}) = \ \mathbf{q}_{xyz}p_w - \mathbf{p}_{xyz}q_w\ \mathbf{1} + p_w q_w \mathbf{1}$	
Perpendicular distance d between point \mathbf{p} and line l . $d(\mathbf{p}, l) = \ \mathbf{l}_v \times \mathbf{p}_{xyz} + p_w \mathbf{l}_m\ \mathbf{1} + \ p_w \mathbf{l}_v\ \mathbf{1}$	
Perpendicular distance d between point \mathbf{p} and plane \mathbf{g} . $d(\mathbf{p}, \mathbf{g}) = (\mathbf{p} \cdot \mathbf{g}) \mathbf{1} + \ p_w \mathbf{g}_{xyz}\ \mathbf{1}$	
Perpendicular distance d between skew lines l and \mathbf{k} . $d(l, \mathbf{k}) = -(\mathbf{l}_v \cdot \mathbf{k}_m + \mathbf{l}_m \cdot \mathbf{k}_v) \mathbf{1} + \ \mathbf{l}_v \times \mathbf{k}_v\ \mathbf{1}$	

Euclidean Angle

Angle Formula	Illustration
<p>Cosine of angle ϕ between planes \mathbf{g} and \mathbf{h}.</p> $\cos \phi(\mathbf{g}, \mathbf{h}) = \frac{(\mathbf{g}_{xyz} \cdot \mathbf{h}_{xyz})}{\ \mathbf{g}\ _0 \ \mathbf{h}\ _0}$	 <p>The diagram shows two blue planes, labeled \mathbf{g} and \mathbf{h}, intersecting at a line. The angle ϕ is shown between the two planes, measured as the angle between their normal vectors.</p>
<p>Cosine of angle ϕ between plane \mathbf{g} and line \mathbf{l}.</p> $\cos \phi(\mathbf{g}, \mathbf{l}) = \frac{\ \mathbf{g}_{xyz} \times \mathbf{l}_v\ }{\ \mathbf{g}\ _0 \ \mathbf{l}\ _0}$	 <p>The diagram shows a blue plane labeled \mathbf{g} and a line labeled \mathbf{l} passing through it. The angle ϕ is shown between the line and the plane, measured as the angle between the line and its projection onto the plane.</p>
<p>Cosine of angle ϕ between lines \mathbf{l} and \mathbf{k}.</p> $\cos \phi(\mathbf{l}, \mathbf{k}) = \frac{(\mathbf{l}_v \cdot \mathbf{k}_v)}{\ \mathbf{l}\ _0 \ \mathbf{k}\ _0}$	 <p>The diagram shows two lines, labeled \mathbf{l} and \mathbf{k}, intersecting at a point. The angle ϕ is shown between the two lines. A dashed line indicates the projection of line \mathbf{l} onto the plane containing line \mathbf{k}.</p>

Bulk and Weight Duals

- Multiply by metric or antimetric, then take complement



\mathbf{u}	$\mathbb{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$
\mathbf{u}^\star	$\mathbb{1}$	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	0	0	0	0	$-\mathbf{e}_{41}$	$-\mathbf{e}_{42}$	$-\mathbf{e}_{43}$	0	0	0	$-\mathbf{e}_4$	0
\mathbf{u}_\star	$\mathbb{1}$	$-\mathbf{e}_{423}$	$-\mathbf{e}_{431}$	$-\mathbf{e}_{412}$	0	0	0	0	$-\mathbf{e}_{41}$	$-\mathbf{e}_{42}$	$-\mathbf{e}_{43}$	0	0	0	\mathbf{e}_4	0
\mathbf{u}^\star	0	0	0	0	\mathbf{e}_{321}	$-\mathbf{e}_{23}$	$-\mathbf{e}_{31}$	$-\mathbf{e}_{12}$	0	0	0	$-\mathbf{e}_1$	$-\mathbf{e}_2$	$-\mathbf{e}_3$	0	$\mathbb{1}$
\mathbf{u}_\star	0	0	0	0	$-\mathbf{e}_{321}$	$-\mathbf{e}_{23}$	$-\mathbf{e}_{31}$	$-\mathbf{e}_{12}$	0	0	0	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	0	$\mathbb{1}$

Hodge Dual

- Right bulk dual is equivalent to Hodge dual

$$\mathbf{u}^\star = \overline{\mathbf{G}\mathbf{u}}$$

- For \mathbf{a} and \mathbf{b} with same grade,

$$\mathbf{a} \wedge \mathbf{b}^\star = (\mathbf{a} \cdot \mathbf{b}) \mathbb{1}$$

Interior Products

- Two exterior products combined with two duals
- Eight *interior* products using right and left duals

- Bulk contraction $\mathbf{a} \vee \mathbf{b}^\star$ $\mathbf{b}_\star \vee \mathbf{a}$

- Weight contraction $\mathbf{a} \vee \mathbf{b}^{\star}$ $\mathbf{b}_\star \vee \mathbf{a}$

- Bulk expansion $\mathbf{a} \wedge \mathbf{b}^\star$ $\mathbf{b}_\star \wedge \mathbf{a}$

- Weight expansion $\mathbf{a} \wedge \mathbf{b}^{\star}$ $\mathbf{b}_\star \wedge \mathbf{a}$

Interior Products

- Right and left interior products differ by grade-dependent sign:

$$\mathbf{b}_* \lrcorner \mathbf{a} = (-1)^{\text{gr}(\mathbf{b})[\text{gr}(\mathbf{a})+\text{gr}(\mathbf{b})]} \mathbf{a} \lrcorner \mathbf{b}^*$$

$$\mathbf{b}_* \wedge \mathbf{a} = (-1)^{\text{ag}(\mathbf{b})[\text{ag}(\mathbf{a})+\text{ag}(\mathbf{b})]} \mathbf{a} \wedge \mathbf{b}^*$$

- Here, $*$ is either \star or \star
- Really need only four interior products

Interior Products

- Interior products reduce to inner products for same grade:

$$\mathbf{a} \vee \mathbf{b}^\star = \mathbf{a} \cdot \mathbf{b}, \quad \text{when } \text{gr}(\mathbf{a}) = \text{gr}(\mathbf{b})$$

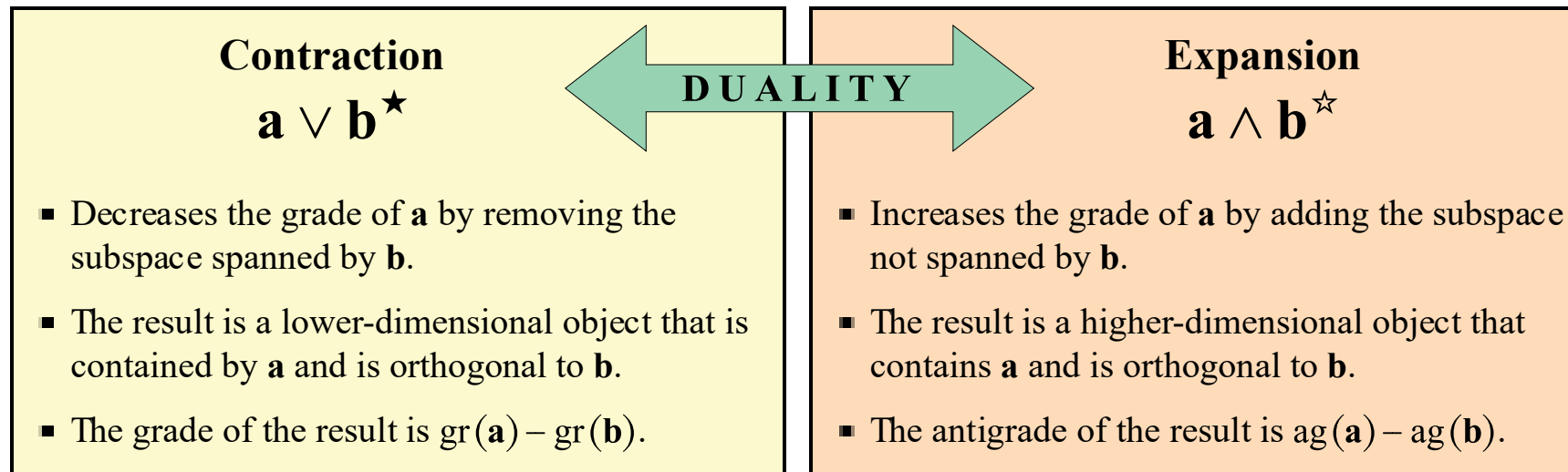
$$\mathbf{a} \vee \mathbf{b}^\star = (\mathbf{a} \circ \mathbf{b}) \vee \mathbf{1}, \quad \text{when } \text{gr}(\mathbf{a}) = \text{gr}(\mathbf{b})$$

$$\mathbf{a} \wedge \mathbf{b}^\star = \mathbf{a} \circ \mathbf{b}, \quad \text{when } \text{ag}(\mathbf{a}) = \text{ag}(\mathbf{b})$$

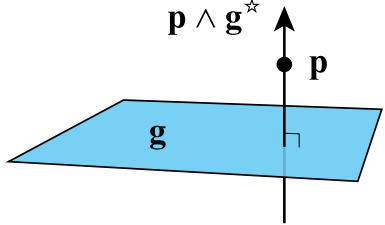
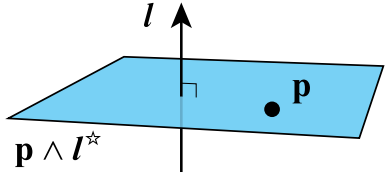
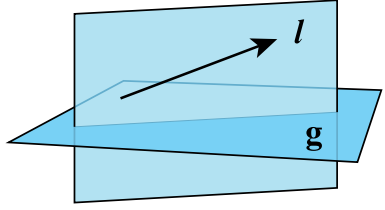
$$\mathbf{a} \wedge \mathbf{b}^\star = (\mathbf{a} \cdot \mathbf{b}) \wedge \mathbf{1}, \quad \text{when } \text{ag}(\mathbf{a}) = \text{ag}(\mathbf{b})$$

Contraction and Expansion

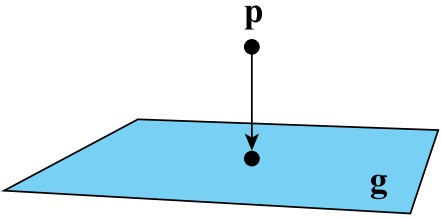
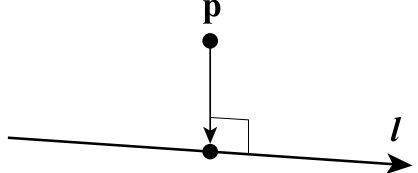
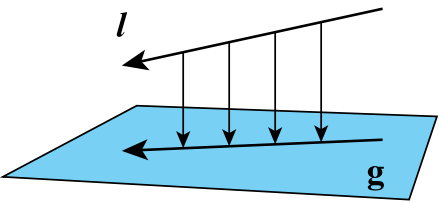
- Subtract grades or antigrades



Weight Expansion

Expansion Operation	Illustration
<p>Line containing point \mathbf{p} and orthogonal to plane \mathbf{g}.</p> $\mathbf{p} \wedge \mathbf{g}^\star = -p_w g_x \mathbf{e}_{41} + (p_z g_y - p_y g_z) \mathbf{e}_{23}$ $- p_w g_y \mathbf{e}_{42} + (p_x g_z - p_z g_x) \mathbf{e}_{31}$ $- p_w g_z \mathbf{e}_{43} + (p_y g_x - p_x g_y) \mathbf{e}_{12}$	
<p>Plane containing point \mathbf{p} and orthogonal to line \mathbf{l}.</p> $\mathbf{p} \wedge \mathbf{l}^\star = -p_w l_{vx} \mathbf{e}_{423} - p_w l_{vy} \mathbf{e}_{431} - p_w l_{vz} \mathbf{e}_{412}$ $+ (p_x l_{vx} + p_y l_{vy} + p_z l_{vz}) \mathbf{e}_{321}$	
<p>Plane containing line \mathbf{l} and orthogonal to plane \mathbf{g}.</p> $\mathbf{l} \wedge \mathbf{g}^\star = (l_{vy} g_z - l_{vz} g_y) \mathbf{e}_{423}$ $+ (l_{vz} g_x - l_{vx} g_z) \mathbf{e}_{431}$ $+ (l_{vx} g_y - l_{vy} g_x) \mathbf{e}_{412}$ $- (l_{mx} g_x + l_{my} g_y + l_{mz} g_z) \mathbf{e}_{321}$	

Orthogonal Projection

Projection Operation	Illustration
<p>Orthogonal projection of point \mathbf{p} onto plane \mathbf{g}.</p> $\mathbf{g} \vee (\mathbf{p} \wedge \mathbf{g}^{\star}) = (g_x^2 + g_y^2 + g_z^2)(p_x \mathbf{e}_1 + p_y \mathbf{e}_2 + p_z \mathbf{e}_3 + p_w \mathbf{e}_4) - (g_x p_x + g_y p_y + g_z p_z + g_w p_w)(g_x \mathbf{e}_1 + g_y \mathbf{e}_2 + g_z \mathbf{e}_3)$	
<p>Orthogonal projection of point \mathbf{p} onto line \mathbf{l}.</p> $\begin{aligned} \mathbf{l} \vee (\mathbf{p} \wedge \mathbf{l}^{\star}) = & (l_{vx} p_x + l_{vy} p_y + l_{vz} p_z)(l_{vx} \mathbf{e}_1 + l_{vy} \mathbf{e}_2 + l_{vz} \mathbf{e}_3) \\ & + (l_{vy} l_{mz} - l_{vz} l_{my}) p_w \mathbf{e}_1 + (l_{vz} l_{mx} - l_{vx} l_{mz}) p_w \mathbf{e}_2 \\ & + (l_{vx} l_{my} - l_{vy} l_{mx}) p_w \mathbf{e}_3 + (l_{vx}^2 + l_{vy}^2 + l_{vz}^2) p_w \mathbf{e}_4 \end{aligned}$	
<p>Orthogonal projection of line \mathbf{l} onto plane \mathbf{g}.</p> $\begin{aligned} \mathbf{g} \vee (\mathbf{l} \wedge \mathbf{g}^{\star}) = & (g_x^2 + g_y^2 + g_z^2)(l_{vx} \mathbf{e}_{41} + l_{vy} \mathbf{e}_{42} + l_{vz} \mathbf{e}_{43}) \\ & - (g_x l_{vx} + g_y l_{vy} + g_z l_{vz})(g_x \mathbf{e}_{41} + g_y \mathbf{e}_{42} + g_z \mathbf{e}_{43}) \\ & + (g_x l_{mx} + g_y l_{my} + g_z l_{mz})(g_x \mathbf{e}_{23} + g_y \mathbf{e}_{31} + g_z \mathbf{e}_{12}) \\ & + (g_z l_{vy} - g_y l_{vz}) g_w \mathbf{e}_{23} + (g_x l_{vz} - g_z l_{vx}) g_w \mathbf{e}_{31} \\ & + (g_y l_{vx} - g_x l_{vy}) g_w \mathbf{e}_{12} \end{aligned}$	

Support

- Orthogonal projection of origin onto line or plane
- Support is point closest to origin contained by object

$$\text{sup}(\mathbf{l}) = (l_{vy}l_{mz} - l_{vz}l_{my})\mathbf{e}_1 + (l_{vz}l_{mx} - l_{vx}l_{mz})\mathbf{e}_2 + (l_{vx}l_{my} - l_{vy}l_{mx})\mathbf{e}_3 + l_v^2\mathbf{e}_4$$

$$\text{sup}(\mathbf{g}) = -g_x g_w \mathbf{e}_1 - g_y g_w \mathbf{e}_2 - g_z g_w \mathbf{e}_3 + (g_x^2 + g_y^2 + g_z^2)\mathbf{e}_4$$

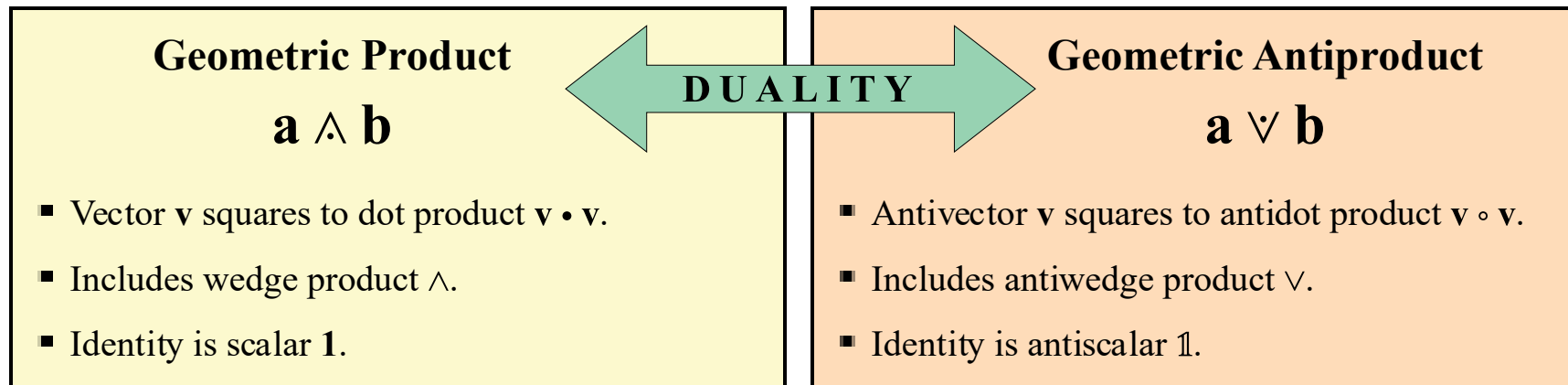
Geometric / Clifford Algebra

- Geometric product $\mathbf{a} \wedge \mathbf{b}$
- Geometric antiproduct $\mathbf{a} \vee \mathbf{b}$
- We use upward and downward wedge with dot inside
- “Wedge-dot” and “Antiwedge-dot”
- G.P. historically denoted by juxtaposition without symbol
- But duality gives us two products that need distinguishing

Geometric Product and Antiproduct

- Vectors square to inner product instead of zero
- Product satisfy the usual De Morgan law

$$\mathbf{a} \vee \mathbf{b} = \overline{\mathbf{a} \wedge \mathbf{b}}$$



Geometric Products

- For vectors \mathbf{a} and \mathbf{b} :

$$\mathbf{a} \wedge \mathbf{b} = \mathbf{a} \wedge \mathbf{b} + \mathbf{a} \cdot \mathbf{b}$$

- For antivectors \mathbf{a} and \mathbf{b} :

$$\mathbf{a} \vee \mathbf{b} = \mathbf{a} \vee \mathbf{b} + \mathbf{a} \circ \mathbf{b}$$

Geometric Products

- For vector \mathbf{a} and arbitrary \mathbf{B} :

$$\mathbf{a} \wedge \mathbf{B} = \mathbf{a} \wedge \mathbf{B} + \mathbf{B} \vee \mathbf{a}^\star$$

- For antivector \mathbf{a} and arbitrary \mathbf{B} :

$$\mathbf{a} \vee \mathbf{B} = \mathbf{a} \vee \mathbf{B} + \mathbf{B} \wedge \mathbf{a}^\star$$

Geometric Products

- In general, there are more terms for **A** and **B** with higher grades
- In 4D algebra, arbitrary **A** and **B** multiply as

$$\mathbf{A} \mathbf{\hat{A}} \mathbf{B} = \mathbf{A} \wedge \mathbf{B} + \mathbf{A} \times \mathbf{B} + \mathbf{A} \cdot \tilde{\mathbf{B}}$$



commutator product

$$\mathbf{A} \times \mathbf{B} = \frac{1}{2}(\mathbf{A} \wedge \mathbf{B} - \mathbf{B} \wedge \mathbf{A})$$

4D Geometric Product

Geometric Product $\mathbf{a} \wedge \mathbf{b}$

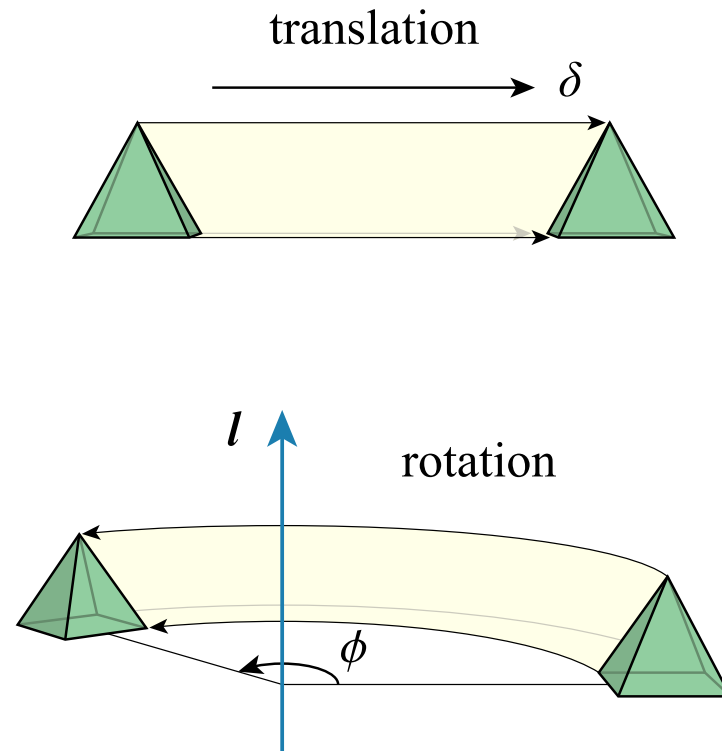
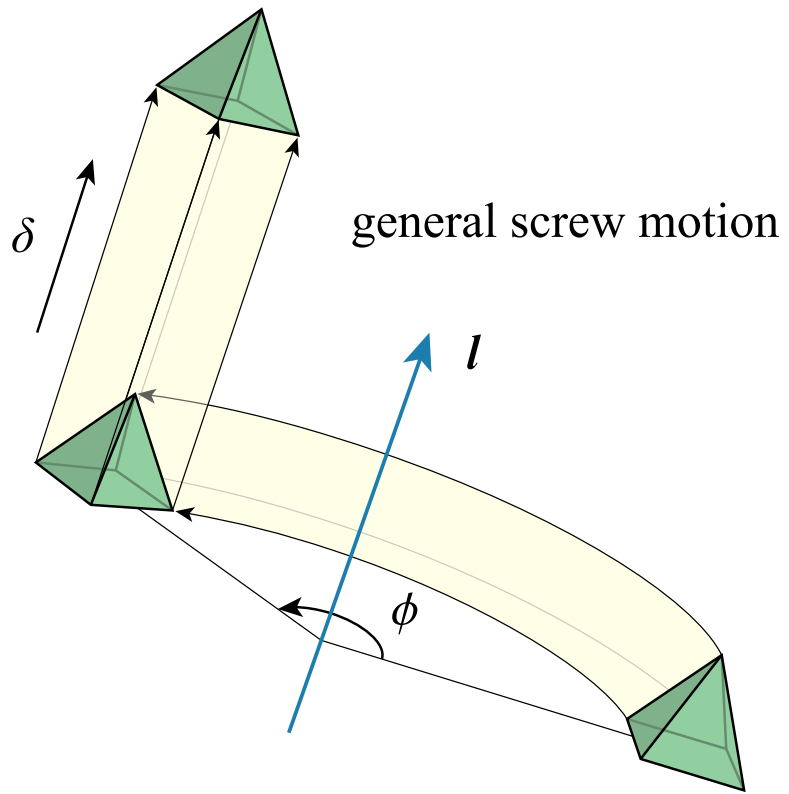
$\mathbf{a} \backslash \mathbf{b}$	$\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$
$\mathbf{1}$	$\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$
\mathbf{e}_1	\mathbf{e}_1	$\mathbf{1}$	\mathbf{e}_{12}	$-\mathbf{e}_{31}$	$-\mathbf{e}_{41}$	$-\mathbf{e}_4$	$-\mathbf{e}_{412}$	\mathbf{e}_{431}	$-\mathbf{e}_{321}$	$-\mathbf{e}_3$	\mathbf{e}_2	$\mathbb{1}$	\mathbf{e}_{43}	$-\mathbf{e}_{42}$	$-\mathbf{e}_{23}$	\mathbf{e}_{423}
\mathbf{e}_2	\mathbf{e}_2	$-\mathbf{e}_{12}$	$\mathbf{1}$	\mathbf{e}_{23}	$-\mathbf{e}_{42}$	\mathbf{e}_{412}	$-\mathbf{e}_4$	$-\mathbf{e}_{423}$	\mathbf{e}_3	$-\mathbf{e}_{321}$	$-\mathbf{e}_1$	$-\mathbf{e}_{43}$	$\mathbb{1}$	\mathbf{e}_{41}	$-\mathbf{e}_{31}$	\mathbf{e}_{431}
\mathbf{e}_3	\mathbf{e}_3	\mathbf{e}_{31}	$-\mathbf{e}_{23}$	$\mathbf{1}$	$-\mathbf{e}_{43}$	$-\mathbf{e}_{431}$	\mathbf{e}_{423}	$-\mathbf{e}_4$	$-\mathbf{e}_2$	\mathbf{e}_1	$-\mathbf{e}_{321}$	\mathbf{e}_{42}	$-\mathbf{e}_{41}$	$\mathbb{1}$	$-\mathbf{e}_{12}$	\mathbf{e}_{412}
\mathbf{e}_4	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	0	0	0	0	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	0	0	0	$\mathbb{1}$	0
\mathbf{e}_{41}	\mathbf{e}_{41}	\mathbf{e}_4	\mathbf{e}_{412}	$-\mathbf{e}_{431}$	0	0	0	0	$-\mathbb{1}$	$-\mathbf{e}_{43}$	\mathbf{e}_{42}	0	0	0	$-\mathbf{e}_{423}$	0
\mathbf{e}_{42}	\mathbf{e}_{42}	$-\mathbf{e}_{412}$	\mathbf{e}_4	\mathbf{e}_{423}	0	0	0	0	\mathbf{e}_{43}	$-\mathbb{1}$	$-\mathbf{e}_{41}$	0	0	0	$-\mathbf{e}_{431}$	0
\mathbf{e}_{43}	\mathbf{e}_{43}	\mathbf{e}_{431}	$-\mathbf{e}_{423}$	\mathbf{e}_4	0	0	0	0	$-\mathbf{e}_{42}$	\mathbf{e}_{41}	$-\mathbb{1}$	0	0	0	$-\mathbf{e}_{412}$	0
\mathbf{e}_{23}	\mathbf{e}_{23}	$-\mathbf{e}_{321}$	$-\mathbf{e}_3$	\mathbf{e}_2	\mathbf{e}_{423}	$-\mathbb{1}$	$-\mathbf{e}_{43}$	\mathbf{e}_{42}	$-\mathbf{1}$	$-\mathbf{e}_{12}$	\mathbf{e}_{31}	$-\mathbf{e}_4$	$-\mathbf{e}_{412}$	\mathbf{e}_{431}	\mathbf{e}_1	\mathbf{e}_{41}
\mathbf{e}_{31}	\mathbf{e}_{31}	\mathbf{e}_3	$-\mathbf{e}_{321}$	$-\mathbf{e}_1$	\mathbf{e}_{431}	\mathbf{e}_{43}	$-\mathbb{1}$	$-\mathbf{e}_{41}$	\mathbf{e}_{12}	$-\mathbf{1}$	$-\mathbf{e}_{23}$	\mathbf{e}_{412}	$-\mathbf{e}_4$	$-\mathbf{e}_{423}$	\mathbf{e}_2	\mathbf{e}_{42}
\mathbf{e}_{12}	\mathbf{e}_{12}	$-\mathbf{e}_2$	\mathbf{e}_1	$-\mathbf{e}_{321}$	\mathbf{e}_{412}	$-\mathbf{e}_{42}$	\mathbf{e}_{41}	$-\mathbb{1}$	$-\mathbf{e}_{31}$	\mathbf{e}_{23}	$-\mathbf{1}$	$-\mathbf{e}_{431}$	\mathbf{e}_{423}	$-\mathbf{e}_4$	\mathbf{e}_3	\mathbf{e}_{43}
\mathbf{e}_{423}	\mathbf{e}_{423}	$-\mathbb{1}$	$-\mathbf{e}_{43}$	\mathbf{e}_{42}	0	0	0	0	$-\mathbf{e}_4$	$-\mathbf{e}_{412}$	\mathbf{e}_{431}	0	0	0	\mathbf{e}_{41}	0
\mathbf{e}_{431}	\mathbf{e}_{431}	\mathbf{e}_{43}	$-\mathbb{1}$	$-\mathbf{e}_{41}$	0	0	0	0	\mathbf{e}_{412}	$-\mathbf{e}_4$	$-\mathbf{e}_{423}$	0	0	0	\mathbf{e}_{42}	0
\mathbf{e}_{412}	\mathbf{e}_{412}	$-\mathbf{e}_{42}$	\mathbf{e}_{41}	$-\mathbb{1}$	0	0	0	0	$-\mathbf{e}_{431}$	\mathbf{e}_{423}	$-\mathbf{e}_4$	0	0	0	\mathbf{e}_{43}	0
\mathbf{e}_{321}	\mathbf{e}_{321}	$-\mathbf{e}_{23}$	$-\mathbf{e}_{31}$	$-\mathbf{e}_{12}$	$-\mathbb{1}$	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	$-\mathbf{e}_{41}$	$-\mathbf{e}_{42}$	$-\mathbf{e}_{43}$	$-\mathbf{1}$	\mathbf{e}_4
$\mathbb{1}$	$\mathbb{1}$	$-\mathbf{e}_{423}$	$-\mathbf{e}_{431}$	$-\mathbf{e}_{412}$	0	0	0	0	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	0	0	0	$-\mathbf{e}_4$	0

4D Geometric Antiproduct

Geometric Antiproduct $\mathbf{a} \vee \mathbf{b}$

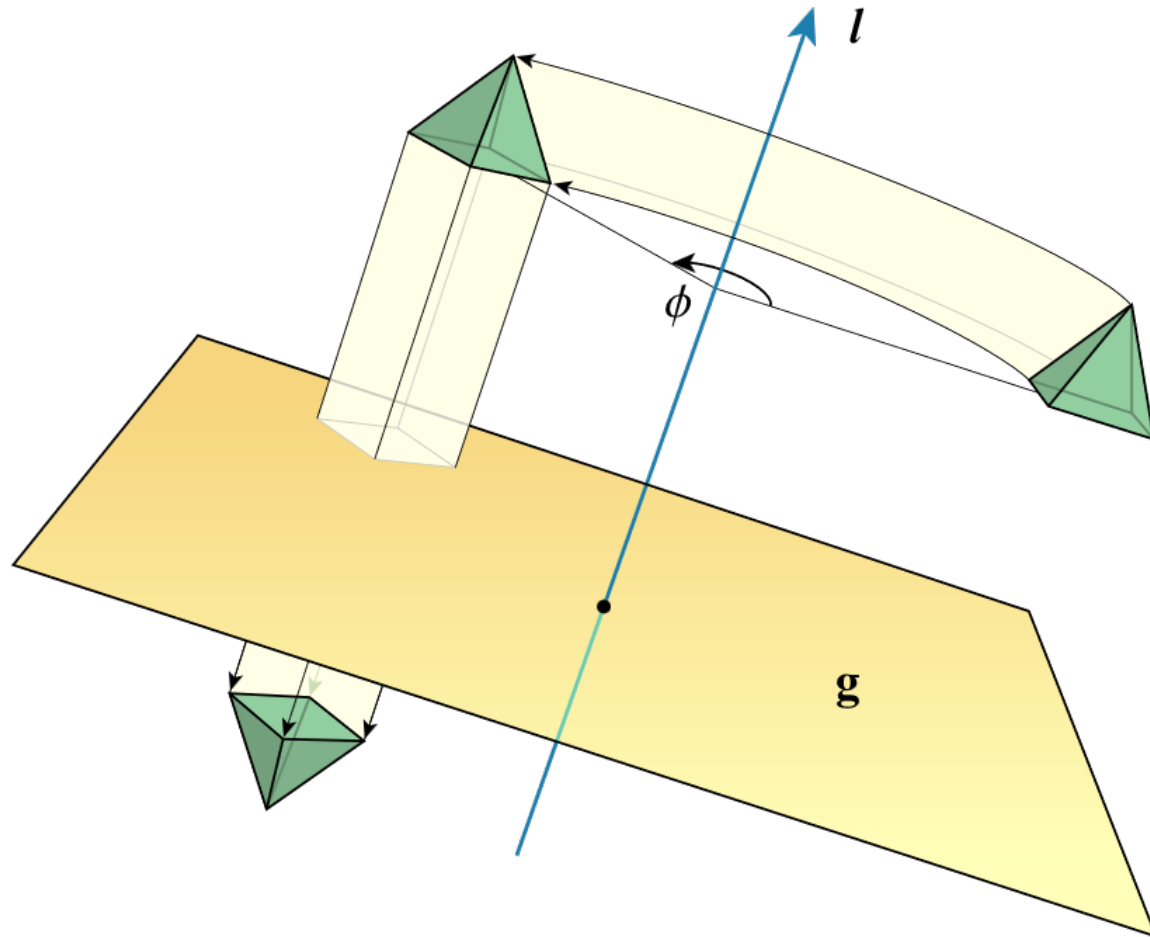
$\mathbf{a} \backslash \mathbf{b}$	$\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$
$\mathbf{1}$	0	0	0	0	\mathbf{e}_{321}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	0	0	0	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	0	$\mathbf{1}$
\mathbf{e}_1	0	0	0	0	$-\mathbf{e}_{23}$	$-\mathbf{e}_{321}$	\mathbf{e}_3	$-\mathbf{e}_2$	0	0	0	$\mathbf{1}$	$-\mathbf{e}_{12}$	\mathbf{e}_{31}	0	\mathbf{e}_1
\mathbf{e}_2	0	0	0	0	$-\mathbf{e}_{31}$	$-\mathbf{e}_3$	$-\mathbf{e}_{321}$	\mathbf{e}_1	0	0	0	\mathbf{e}_{12}	$\mathbf{1}$	$-\mathbf{e}_{23}$	0	\mathbf{e}_2
\mathbf{e}_3	0	0	0	0	$-\mathbf{e}_{12}$	\mathbf{e}_2	$-\mathbf{e}_1$	$-\mathbf{e}_{321}$	0	0	0	$-\mathbf{e}_{31}$	\mathbf{e}_{23}	$\mathbf{1}$	0	\mathbf{e}_3
\mathbf{e}_4	$-\mathbf{e}_{321}$	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	$-\mathbb{1}$	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	$-\mathbf{e}_1$	$-\mathbf{e}_2$	$-\mathbf{e}_3$	$-\mathbf{e}_{41}$	$-\mathbf{e}_{42}$	$-\mathbf{e}_{43}$	$\mathbf{1}$	\mathbf{e}_4
\mathbf{e}_{41}	\mathbf{e}_{23}	$-\mathbf{e}_{321}$	\mathbf{e}_3	$-\mathbf{e}_2$	\mathbf{e}_{423}	$-\mathbb{1}$	\mathbf{e}_{43}	$-\mathbf{e}_{42}$	$-\mathbf{1}$	\mathbf{e}_{12}	$-\mathbf{e}_{31}$	$-\mathbf{e}_4$	\mathbf{e}_{412}	$-\mathbf{e}_{431}$	\mathbf{e}_1	\mathbf{e}_{41}
\mathbf{e}_{42}	\mathbf{e}_{31}	$-\mathbf{e}_3$	$-\mathbf{e}_{321}$	\mathbf{e}_1	\mathbf{e}_{431}	$-\mathbf{e}_{43}$	$-\mathbb{1}$	\mathbf{e}_{41}	$-\mathbf{e}_{12}$	$-\mathbf{1}$	\mathbf{e}_{23}	$-\mathbf{e}_{412}$	$-\mathbf{e}_4$	\mathbf{e}_{423}	\mathbf{e}_2	\mathbf{e}_{42}
\mathbf{e}_{43}	\mathbf{e}_{12}	\mathbf{e}_2	$-\mathbf{e}_1$	$-\mathbf{e}_{321}$	\mathbf{e}_{412}	\mathbf{e}_{42}	$-\mathbf{e}_{41}$	$-\mathbb{1}$	\mathbf{e}_{31}	$-\mathbf{e}_{23}$	$-\mathbf{1}$	\mathbf{e}_{431}	$-\mathbf{e}_{423}$	$-\mathbf{e}_4$	\mathbf{e}_3	\mathbf{e}_{43}
\mathbf{e}_{23}	0	0	0	0	\mathbf{e}_1	$-\mathbf{1}$	\mathbf{e}_{12}	$-\mathbf{e}_{31}$	0	0	0	$-\mathbf{e}_{321}$	\mathbf{e}_3	$-\mathbf{e}_2$	0	\mathbf{e}_{23}
\mathbf{e}_{31}	0	0	0	0	\mathbf{e}_2	$-\mathbf{e}_{12}$	$-\mathbf{1}$	\mathbf{e}_{23}	0	0	0	$-\mathbf{e}_3$	$-\mathbf{e}_{321}$	\mathbf{e}_1	0	\mathbf{e}_{31}
\mathbf{e}_{12}	0	0	0	0	\mathbf{e}_3	\mathbf{e}_{31}	$-\mathbf{e}_{23}$	$-\mathbf{1}$	0	0	0	\mathbf{e}_2	$-\mathbf{e}_1$	$-\mathbf{e}_{321}$	0	\mathbf{e}_{12}
\mathbf{e}_{423}	$-\mathbf{e}_1$	$-\mathbf{1}$	\mathbf{e}_{12}	$-\mathbf{e}_{31}$	$-\mathbf{e}_{41}$	$-\mathbf{e}_4$	\mathbf{e}_{412}	$-\mathbf{e}_{431}$	\mathbf{e}_{321}	$-\mathbf{e}_3$	\mathbf{e}_2	$\mathbb{1}$	$-\mathbf{e}_{43}$	\mathbf{e}_{42}	\mathbf{e}_{23}	\mathbf{e}_{423}
\mathbf{e}_{431}	$-\mathbf{e}_2$	$-\mathbf{e}_{12}$	$-\mathbf{1}$	\mathbf{e}_{23}	$-\mathbf{e}_{42}$	$-\mathbf{e}_{412}$	$-\mathbf{e}_4$	\mathbf{e}_{423}	\mathbf{e}_3	\mathbf{e}_{321}	$-\mathbf{e}_1$	\mathbf{e}_{43}	$\mathbb{1}$	$-\mathbf{e}_{41}$	\mathbf{e}_{31}	\mathbf{e}_{431}
\mathbf{e}_{412}	$-\mathbf{e}_3$	\mathbf{e}_{31}	$-\mathbf{e}_{23}$	$-\mathbf{1}$	$-\mathbf{e}_{43}$	\mathbf{e}_{431}	$-\mathbf{e}_{423}$	$-\mathbf{e}_4$	$-\mathbf{e}_2$	\mathbf{e}_1	\mathbf{e}_{321}	$-\mathbf{e}_{42}$	\mathbf{e}_{41}	$\mathbb{1}$	\mathbf{e}_{12}	\mathbf{e}_{412}
\mathbf{e}_{321}	0	0	0	0	$-\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	0	0	0	$-\mathbf{e}_{23}$	$-\mathbf{e}_{31}$	$-\mathbf{e}_{12}$	0	\mathbf{e}_{321}
$\mathbb{1}$	$\mathbf{1}$	\mathbf{e}_1	\mathbf{e}_2	\mathbf{e}_3	\mathbf{e}_4	\mathbf{e}_{41}	\mathbf{e}_{42}	\mathbf{e}_{43}	\mathbf{e}_{23}	\mathbf{e}_{31}	\mathbf{e}_{12}	\mathbf{e}_{423}	\mathbf{e}_{431}	\mathbf{e}_{412}	\mathbf{e}_{321}	$\mathbb{1}$

Proper Euclidean Isometries

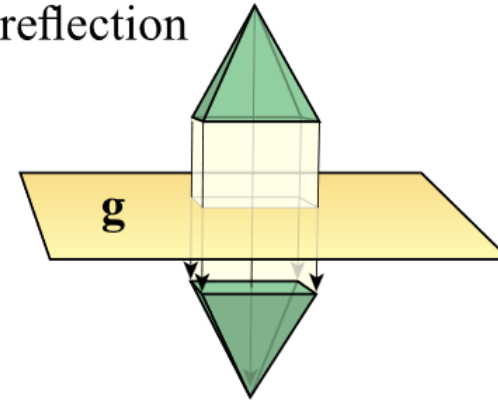


Improper Euclidean Isometries

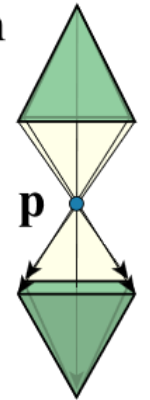
general rotoreflection



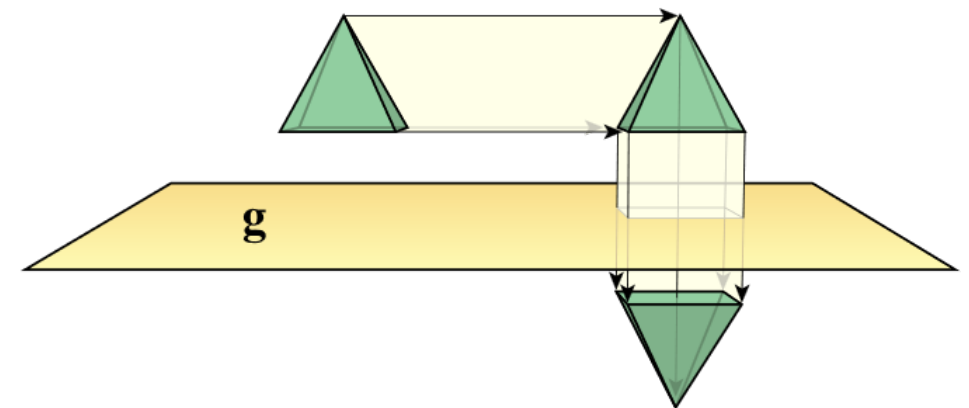
reflection



inversion



transflection



Geometric Product

- Geometric **product** in 4D space fixes the origin
- Cannot perform transformations we want

- Geometric **antiproduct** performs Euclidean isometries
- Uses sandwiching similar to quaternions

Plane Reflection

- Sandwich antiproduct with plane \mathbf{g} performs reflection:

$$\mathbf{u}' = \mathbf{g} \vee \mathbf{u} \vee \mathbf{g}$$

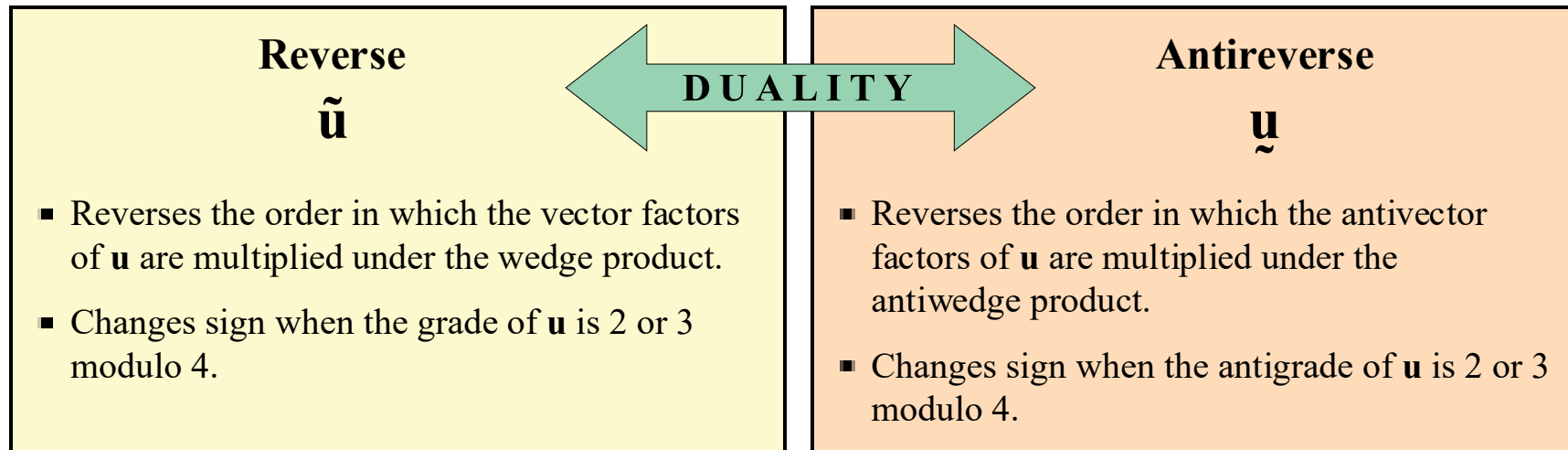
- Multiple reflections stack outward from \mathbf{u} :

$$\mathbf{u}' = (\mathbf{h} \vee \mathbf{g}) \vee \mathbf{u} \vee (\mathbf{g} \vee \mathbf{h})$$

- Basis for all Euclidean isometries

Reverse and Antireverse

- Multiply vector or antivector factors in reverse order

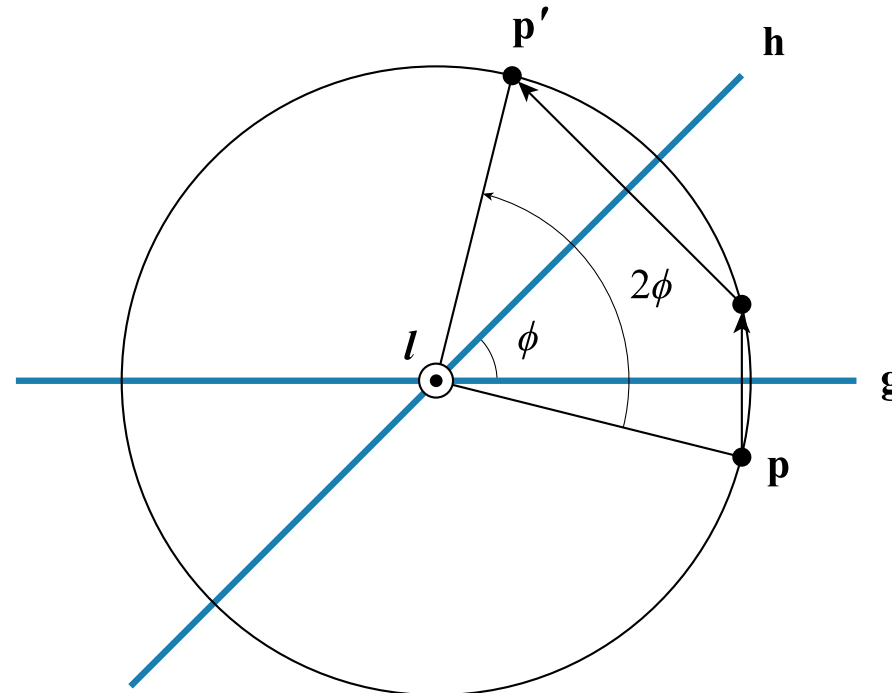


u	1	e₁	e₂	e₃	e₄	e₄₁	e₄₂	e₄₃	e₂₃	e₃₁	e₁₂	e₄₂₃	e₄₃₁	e₄₁₂	e₃₂₁	1
u-tilde	1	e₁	e₂	e₃	e₄	-e₄₁	-e₄₂	-e₄₃	-e₂₃	-e₃₁	-e₁₂	-e₄₂₃	-e₄₃₁	-e₄₁₂	-e₃₂₁	1
u-tilde	1	-e₁	-e₂	-e₃	-e₄	-e₄₁	-e₄₂	-e₄₃	-e₂₃	-e₃₁	-e₁₂	e₄₂₃	e₄₃₁	e₄₁₂	e₃₂₁	1

Rotation about a Line

- Let \mathbf{g} and \mathbf{h} be planes meeting at an angle ϕ
- Reflection across \mathbf{g} followed by \mathbf{h} is rotation through 2ϕ about line l where planes intersect

$$l = \frac{\mathbf{h} \vee \mathbf{g}}{\|\mathbf{h} \vee \mathbf{g}\|_o}$$



Rotation about a Line

- Planes multiply together under geometric antiproduct to form rotation operator \mathbf{R}

$$\mathbf{p}' = \mathbf{h} \vee (\mathbf{g} \vee \mathbf{p} \vee \mathbf{g}) \vee \mathbf{h}$$

$$\mathbf{p}' = \mathbf{R} \vee \mathbf{p} \vee \mathbf{R}$$

$$\mathbf{R} = \mathbf{h} \vee \mathbf{g}$$

Rotation about a Line

- General form of rotation operator \mathbf{R} :

$$\mathbf{R} = l \sin \phi + \mathbb{1} \cos \phi$$

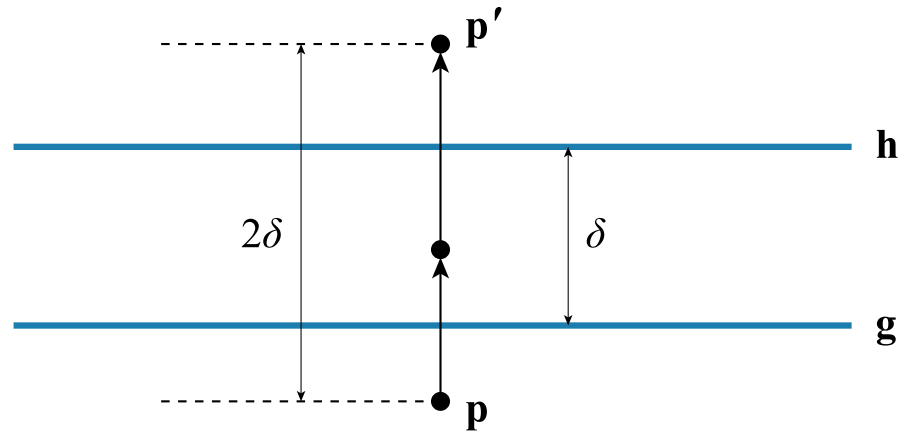
- Rotates through angle 2ϕ about unitized line l

$$\mathbf{u}' = \mathbf{R} \mathbf{u} \mathbf{R}$$

- Rotates any geometry and even other operators

Translation

- If planes **g** and **h** are parallel, result is a translation
- Translation goes along normal direction by twice the distance δ between the planes



Translation

- General form of translation operator \mathbf{T} :

$$\mathbf{T} = \tau_x \mathbf{e}_{23} + \tau_y \mathbf{e}_{31} + \tau_z \mathbf{e}_{12} + \mathbb{1}$$

- Translates by displacement vector 2τ

$$\mathbf{u}' = \mathbf{T} \mathbf{u} \mathbf{T}$$

- Translates any geometry and even other operators

Euclidean Isometry Operators

- Sandwiches with geometric antiproduct perform Euclidean isometries
- Motor = MOtion operaTOR
- Flector = reFLEction operaTOR

Motor

- General form of a motor:

$$\mathbf{Q} = Q_{vx} \mathbf{e}_{41} + Q_{vy} \mathbf{e}_{42} + Q_{vz} \mathbf{e}_{43} + Q_{vw} \mathbf{1} + Q_{mx} \mathbf{e}_{23} + Q_{my} \mathbf{e}_{31} + Q_{mz} \mathbf{e}_{12} + Q_{mw} \mathbf{1}$$

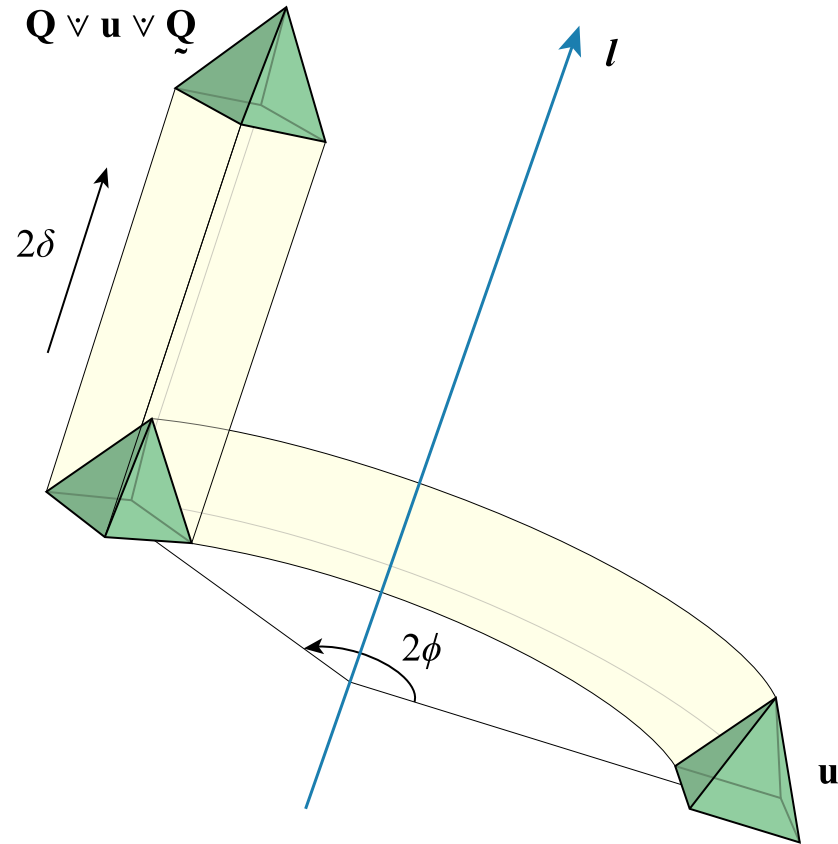
Rotation Quaternion

Moment and Displacement

- Performs any combination of rotations and translations

$$\mathbf{u}' = \mathbf{Q} \vee \mathbf{u} \vee \tilde{\mathbf{Q}}$$

Motor



$$\mathbf{Q} = \exp_{\vee}[(\delta \mathbf{1} + \phi \mathbf{1}) \vee \mathbf{l}] = \mathbf{l} \sin \phi - \mathbf{l}^{\star} \delta \cos \phi - \delta \sin \phi + \mathbf{1} \cos \phi$$

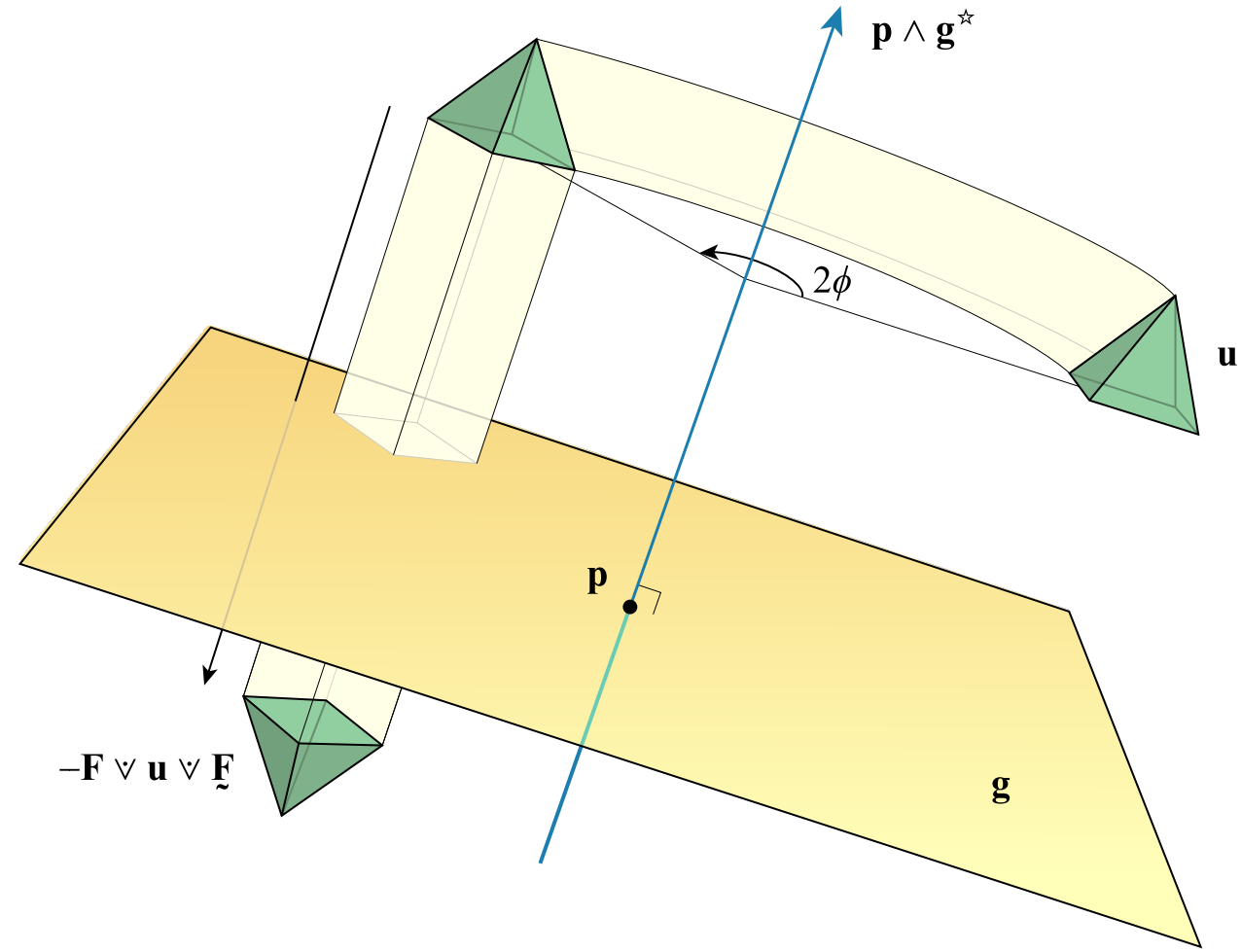
Flector

- General form of a flector:

$$\mathbf{F} = \underbrace{F_{px} \mathbf{e}_1 + F_{py} \mathbf{e}_2 + F_{pz} \mathbf{e}_3 + F_{pw} \mathbf{e}_4}_{\text{Point}} + \underbrace{F_{gx} \mathbf{e}_{423} + F_{gy} \mathbf{e}_{431} + F_{gz} \mathbf{e}_{412} + F_{gw} \mathbf{e}_{321}}_{\text{Plane}}$$

- Performs any combination of roto reflections

Flector



$$\mathbf{F} = \mathbf{p} \sin \phi + \mathbf{g} \cos \phi$$

Motor Parameterization

- A motion operator is parameterized by:
 - A unitized line l
 - A rotation angle ϕ
 - A displacement distance δ

- Exponential with respect to geometric antiproduct:

$$\mathbf{Q} = \exp_{\vee}[(\delta\mathbf{1} + \phi\mathbf{1}) \vee l] = l \sin \phi - l^{\star} \delta \cos \phi - \delta \sin \phi + \mathbf{1} \cos \phi$$

- $\delta\mathbf{1} + \phi\mathbf{1}$ is *pitch* of screw transformation

Motor Parameterization

- Given arbitrary motor \mathbf{Q} , can calculate parameters

$$\mathbf{Q} = Q_{vx} \mathbf{e}_{41} + Q_{vy} \mathbf{e}_{42} + Q_{vz} \mathbf{e}_{43} + Q_{vw} \mathbb{1} + Q_{mx} \mathbf{e}_{23} + Q_{my} \mathbf{e}_{31} + Q_{mz} \mathbf{e}_{12} + Q_{mw} \mathbf{1}$$

$$\mathbf{Q} = \exp_{\vee} [(\delta \mathbf{1} + \phi \mathbb{1}) \vee \mathbf{l}] = \mathbf{l} \sin \phi - \mathbf{l}^{\star} \delta \cos \phi - \delta \sin \phi + \mathbb{1} \cos \phi$$

$$s = \sin \phi = \sqrt{1 - Q_{vw}^2} \quad \delta = -\frac{Q_{mw}}{s} \quad \phi = \tan^{-1} \left(\frac{s}{Q_{vw}} \right)$$

$$\mathbf{l}_{\vee} = \frac{1}{s} \mathbf{Q}_{vxyz} \quad \mathbf{l}_{\mathbf{m}} = \frac{1}{s} \left(\mathbf{Q}_{mxyz} + \frac{Q_{vw} Q_{mw}}{s^2} \mathbf{Q}_{vxyz} \right)$$

Operator Norms

- Geometric norm of operator is half the distance origin is moved by the operator

$$\|\mathbf{Q}\| = \frac{1}{2} \sqrt{Q_{mx}^2 + Q_{my}^2 + Q_{mz}^2 + Q_{mw}^2} + \frac{1}{2} \sqrt{Q_{vx}^2 + Q_{vy}^2 + Q_{vz}^2 + Q_{vw}^2}$$

Motor Interpolation

- To interpolate from motor \mathbf{Q}_1 to motor \mathbf{Q}_2 , first calculate

$$\mathbf{Q}_0 = \mathbf{Q}_2 \vee \mathbf{Q}_1^{-1} = \mathbf{Q}_2 \vee \mathbf{Q}_1$$

- Then calculate parameters l , δ , and ϕ for \mathbf{Q}_0
- Interpolate from identity $\mathbb{1}$ to \mathbf{Q}_0 with

$$\mathbf{Q}(t) = \exp_{\vee} [t(\delta \mathbf{1} + \phi \mathbf{1}) \vee l] = l \sin(t\phi) - l^{\star} t \delta \cos(t\phi) - t \delta \sin(t\phi) + \mathbf{1} \cos(t\phi)$$

- Finally, calculate $\mathbf{Q}(t) \vee \mathbf{Q}_1$

Motor Interpolation

- That can be computationally expensive
- Approximate interpolation is often acceptable:

$$\mathbf{Q}(t) = (1 - t)\mathbf{Q}_1 + t\mathbf{Q}_2$$

- This needs to be unitized and constrained

$$\frac{\mathbf{Q}}{\|\mathbf{Q}_v\|} \vee \left(-\frac{\mathbf{Q}_v \cdot \mathbf{Q}_m}{\mathbf{Q}_v^2} \mathbf{1} + \mathbb{1} \right) = \frac{1}{\|\mathbf{Q}_v\|} \left[\mathbf{Q} - \frac{\mathbf{Q}_v \cdot \mathbf{Q}_m}{\mathbf{Q}_v^2} (\mathcal{Q}_{vx} \mathbf{e}_{23} + \mathcal{Q}_{vy} \mathbf{e}_{31} + \mathcal{Q}_{vz} \mathbf{e}_{12} + \mathcal{Q}_{vw}) \right]$$

Square Root of Motor

- Special case of interpolation from $\mathbb{1}$ to \mathbf{Q} when $t = 1/2$

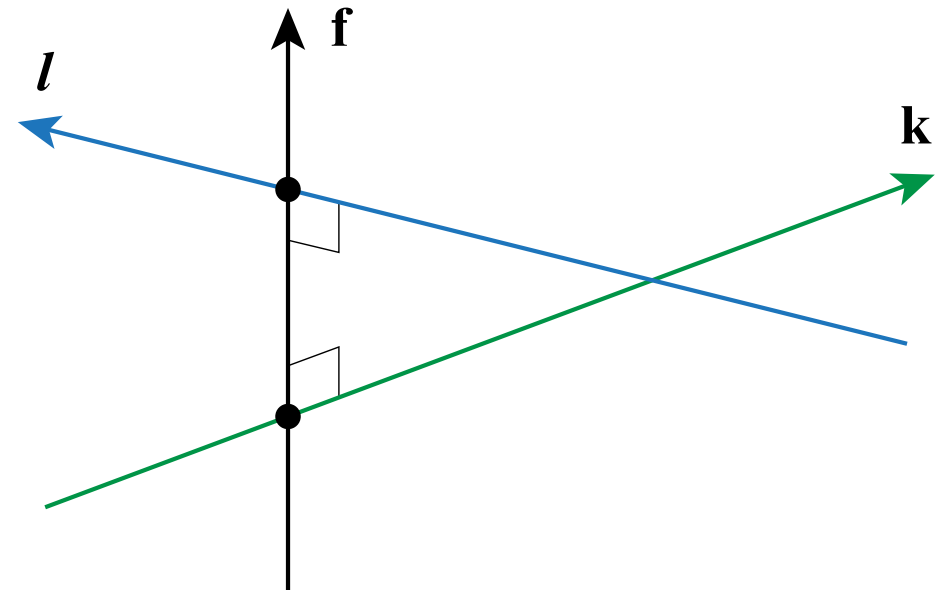
$$\sqrt[2]{\mathbf{Q}} = \frac{\mathbf{Q} + \mathbb{1}}{\sqrt{2 + 2Q_1}} \vee \left(\mathbb{1} - \frac{Q_1}{2 + 2Q_1} \mathbf{1} \right)$$

- For simple motor (pure rotation or translation), this simplifies:

$$\sqrt[2]{\mathbf{Q}} = \frac{\mathbf{Q} + \mathbb{1}}{\|\mathbf{Q} + \mathbb{1}\|_o}$$

Line to Line Motion

- Let \mathbf{k} and l be lines separated by distance δ with angle ϕ between directions
- Operator $l \vee \mathbf{k}$ rotates by 2ϕ and translates by distance 2δ about line \mathbf{f} connecting closest points
- Square root of this operator transforms line \mathbf{k} into line l



Motor-Point Transformation

- 25 multiply-adds:

$$\mathbf{p}'_{xyz} = \mathbf{p}_{xyz} + 2(Q_{vw}\mathbf{a} + \mathbf{v} \times \mathbf{a} - Q_{mw}p_w\mathbf{v})$$

$$p'_w = p_w$$

$$\mathbf{a} = \mathbf{v} \times \mathbf{p}_{xyz} + p_w\mathbf{m}$$

$$\mathbf{v} = (Q_{vx}, Q_{vy}, Q_{vz})$$

$$\mathbf{m} = (Q_{mx}, Q_{my}, Q_{mz})$$

- 3×4 matrix transformation only requires 12 multiply-adds, (or just 9 if $p_w = 1$)

Motor-Line Transformation

- 54 multiply-adds:

$$l'_v = l_v + 2(Q_{vw}\mathbf{a} + \mathbf{v} \times \mathbf{a})$$

$$l'_m = l_m + 2[Q_{mw}\mathbf{a} + Q_{vw}(\mathbf{b} + \mathbf{c}) + \mathbf{v} \times (\mathbf{b} + \mathbf{c}) + \mathbf{m} \times \mathbf{a}]$$

$$\mathbf{a} = \mathbf{v} \times l_v \quad \mathbf{b} = \mathbf{v} \times l_m \quad \mathbf{c} = \mathbf{m} \times l_v$$

- 6×6 matrix transformation only requires 27 multiply-adds

Motor-Plane Transformation

- 35 multiply-adds:

$$\mathbf{g}'_{xyz} = \mathbf{g}_{xyz} + 2(Q_{vw}\mathbf{a} + \mathbf{v} \times \mathbf{a})$$

$$g'_w = g_w + 2\left[(\mathbf{m} \times \mathbf{g}_{xyz} + Q_{mw}\mathbf{g}_{xyz}) \cdot \mathbf{v} - Q_{vw}(\mathbf{m} \cdot \mathbf{g}_{xyz})\right]$$

$$\mathbf{a} = \mathbf{v} \times \mathbf{g}_{xyz}$$

- 4×4 matrix transformation only requires 13 multiply-adds

Motor to Matrix

$$\mathbf{A}_Q = \begin{bmatrix} 1 - 2(Q_{vy}^2 + Q_{vz}^2) & 2Q_{vx}Q_{vy} & 2Q_{vz}Q_{vx} & 2(Q_{vy}Q_{mz} - Q_{vz}Q_{my}) \\ 2Q_{vx}Q_{vy} & 1 - 2(Q_{vz}^2 + Q_{vx}^2) & 2Q_{vy}Q_{vz} & 2(Q_{vz}Q_{mx} - Q_{vx}Q_{mz}) \\ 2Q_{vz}Q_{vx} & 2Q_{vy}Q_{vz} & 1 - 2(Q_{vx}^2 + Q_{vy}^2) & 2(Q_{vx}Q_{my} - Q_{vy}Q_{mx}) \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{B}_Q = \begin{bmatrix} 0 & -2Q_{vz}Q_{vw} & 2Q_{vy}Q_{vw} & 2(Q_{vw}Q_{mx} - Q_{vx}Q_{mw}) \\ 2Q_{vz}Q_{vw} & 0 & -2Q_{vx}Q_{vw} & 2(Q_{vw}Q_{my} - Q_{vy}Q_{mw}) \\ -2Q_{vy}Q_{vw} & 2Q_{vx}Q_{vw} & 0 & 2(Q_{vw}Q_{mz} - Q_{vz}Q_{mw}) \\ 0 & 0 & 0 & 0 \end{bmatrix}$$

$$\mathbf{M}_Q = \mathbf{A}_Q + \mathbf{B}_Q$$

$$\mathbf{M}_Q^{-1} = \mathbf{A}_Q - \mathbf{B}_Q$$

Motor Composition

- 48 multiply-adds:

$$\begin{aligned}\mathbf{Q} \vee \mathbf{R} = & (Q_{vw}R_{vx} + Q_{vx}R_{vw} + Q_{vy}R_{vz} - Q_{vz}R_{vy})\mathbf{e}_{41} \\ & + (Q_{vw}R_{vy} - Q_{vx}R_{vz} + Q_{vy}R_{vw} + Q_{vz}R_{vx})\mathbf{e}_{42} \\ & + (Q_{vw}R_{vz} + Q_{vx}R_{vy} - Q_{vy}R_{vx} + Q_{vz}R_{vw})\mathbf{e}_{43} \\ & + (Q_{vw}R_{vw} - Q_{vx}R_{vx} - Q_{vy}R_{vy} - Q_{vz}R_{vz})\mathbf{1} \\ & + (Q_{mw}R_{vx} + Q_{mx}R_{vw} + Q_{my}R_{vz} - Q_{mz}R_{vy} + Q_{vw}R_{mx} + Q_{vx}R_{mw} + Q_{vy}R_{mz} - Q_{vz}R_{my})\mathbf{e}_{23} \\ & + (Q_{mw}R_{vy} - Q_{mx}R_{vz} + Q_{my}R_{vw} + Q_{mz}R_{vx} + Q_{vw}R_{my} - Q_{vx}R_{mz} + Q_{vy}R_{mw} + Q_{vz}R_{mx})\mathbf{e}_{31} \\ & + (Q_{mw}R_{vz} + Q_{mx}R_{vy} - Q_{my}R_{vx} + Q_{mz}R_{vw} + Q_{vw}R_{mz} + Q_{vx}R_{my} - Q_{vy}R_{mx} + Q_{vz}R_{mw})\mathbf{e}_{12} \\ & + (Q_{mw}R_{vw} - Q_{mx}R_{vx} - Q_{my}R_{vy} - Q_{mz}R_{vz} + Q_{vw}R_{mw} - Q_{vx}R_{mx} - Q_{vy}R_{my} + Q_{vz}R_{mz})\mathbf{1}\end{aligned}$$

- Composition of equivalent 3×4 matrices requires 33 multiply-adds

Motor and Matrix

$$\mathbf{M} = \begin{bmatrix} m_{11} & m_{12} & m_{13} & t_x \\ m_{21} & m_{22} & m_{23} & t_y \\ m_{31} & m_{32} & m_{33} & t_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{Q} = Q_{vx} \mathbf{e}_{41} + Q_{vy} \mathbf{e}_{42} + Q_{vz} \mathbf{e}_{43} + Q_{vw} \mathbf{1} + Q_{mx} \mathbf{e}_{23} + Q_{my} \mathbf{e}_{31} + Q_{mz} \mathbf{e}_{12} + Q_{mw} \mathbf{1}$$

$$\mathbf{M} = \begin{bmatrix} 1 - 2(Q_{vy}^2 + Q_{vz}^2) & 2(Q_{vx}Q_{vy} - Q_{vz}Q_{vw}) & 2(Q_{vz}Q_{vx} + Q_{vy}Q_{vw}) & 2(Q_{vy}Q_{mz} - Q_{vz}Q_{my} + Q_{vw}Q_{mx} - Q_{vx}Q_{mw}) \\ 2(Q_{vx}Q_{vy} + Q_{vz}Q_{vw}) & 1 - 2(Q_{vz}^2 + Q_{vx}^2) & 2(Q_{vy}Q_{vz} - Q_{vx}Q_{vw}) & 2(Q_{vz}Q_{mx} - Q_{vx}Q_{mz} + Q_{vw}Q_{my} - Q_{vy}Q_{mw}) \\ 2(Q_{vz}Q_{vx} - Q_{vy}Q_{vw}) & 2(Q_{vy}Q_{vz} + Q_{vx}Q_{vw}) & 1 - 2(Q_{vx}^2 + Q_{vy}^2) & 2(Q_{vx}Q_{my} - Q_{vy}Q_{mx} + Q_{vw}Q_{mz} - Q_{vz}Q_{mw}) \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

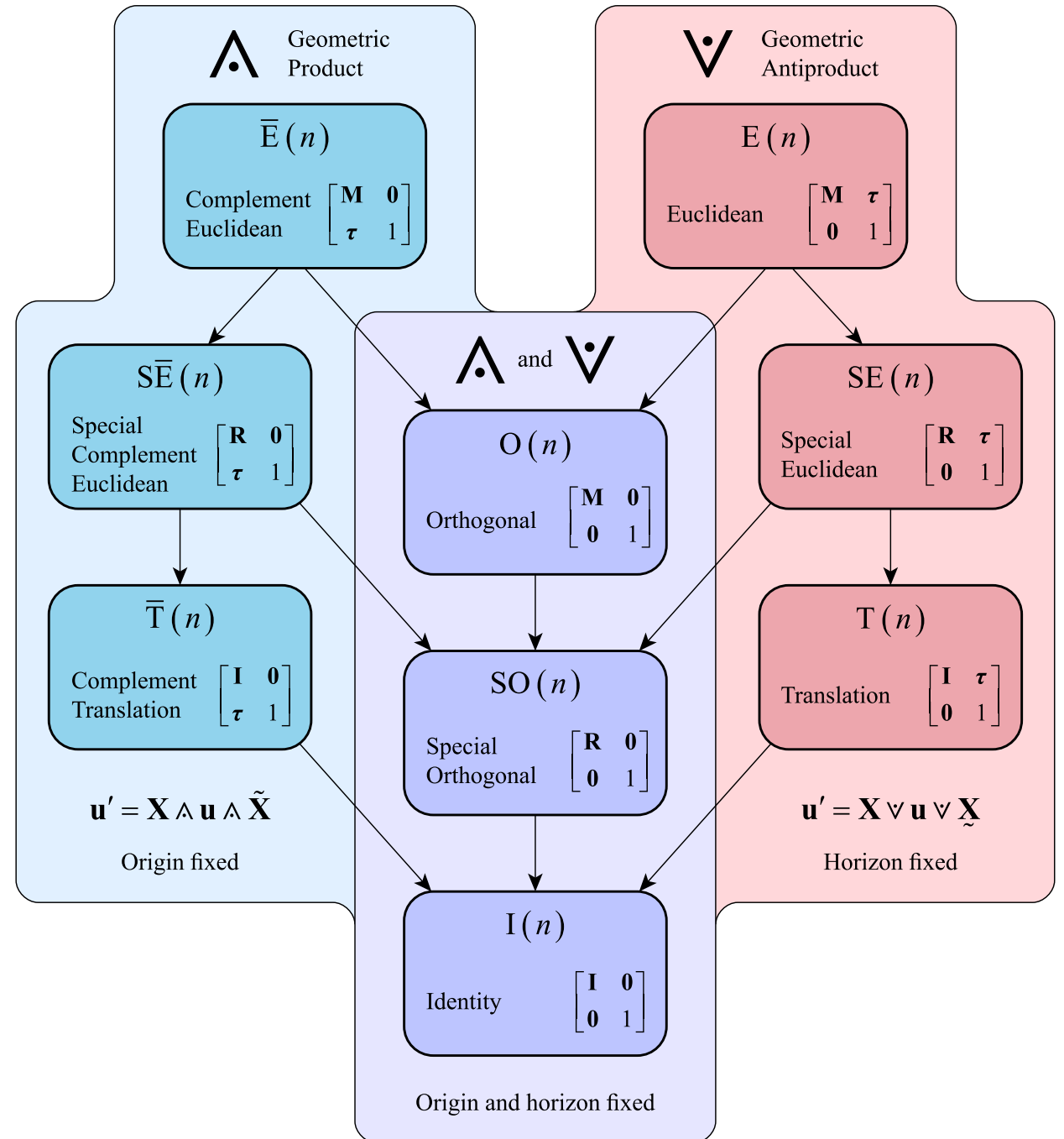
Matrix Advantages

- Can represent more transformations
- Can read off origin and axis directions in transformed space
- Faster to transform objects
- Faster to compose

Motor Advantages

- Smaller storage requirements
 - Usually 8 floats, but can reduce to 6
- Inversion is trivial
 - Just reverse, negating six bivector components
- Better parameterization
- Better interpolation properties

Transformation Groups



Transwedge Product

- Generalization of exterior and interior products

$$\mathbf{a} \underset{k}{\mathbb{A}} \mathbf{b} = \sum_{c \in \mathcal{B}_k} (\underline{\mathbf{c}} \vee \mathbf{a}) \wedge (\mathbf{b} \vee \mathbf{c}^\star)$$

$$\mathbf{a} \underset{k}{\mathbb{A}} \mathbf{b} = \sum_{c \in \mathcal{B}_k} (\mathbf{c}^\star \vee \mathbf{a}) \wedge (\mathbf{b} \vee \bar{\mathbf{c}})$$

\mathcal{B}_k = set of basis elements of grade k

Transwedge Product

- Order 0 transwedge product is the exterior product:

$$\mathbf{a} \underset{0}{\mathbb{A}} \mathbf{b} = \mathbf{a} \wedge \mathbf{b}$$

- Order m transwedge product is the interior product, where m is minimum grade of operands

$$\mathbf{a} \underset{\min(\text{gr}(\mathbf{a}), \text{gr}(\mathbf{b}))}{\mathbb{A}} \mathbf{b} = \begin{cases} \mathbf{b} \vee \mathbf{a}^\star, & \text{if } \text{gr}(\mathbf{a}) \leq \text{gr}(\mathbf{b}); \\ \mathbf{b}_\star \vee \mathbf{a}, & \text{if } \text{gr}(\mathbf{a}) \geq \text{gr}(\mathbf{b}). \end{cases}$$

Transwedge Product

- Orders in between 0 and m , exclusive, are “liminal” products
 - Neither exterior nor interior
- Geometric product decomposes into transwedge products as

$$\mathbf{a} \wedge \mathbf{b} = \sum_{k=0}^m (-1)^{k(k-1)/2} \mathbf{a} \underset{k}{\wedge} \mathbf{b}$$

Transwedge Product

Transwedge Products

 $a \wedge b$
 $a \wedge_1 b$
 $-a \wedge_2 b$
 $-a \wedge_3 b$
 $a \wedge_4 b$

a \ b	1	e₁	e₂	e₃	e₄	e₄₁	e₄₂	e₄₃	e₂₃	e₃₁	e₁₂	e₄₂₃	e₄₃₁	e₄₁₂	e₃₂₁	1
1	1	e₁	e₂	e₃	e₄	e₄₁	e₄₂	e₄₃	e₂₃	e₃₁	e₁₂	e₄₂₃	e₄₃₁	e₄₁₂	e₃₂₁	1
e₁	e₁	1	e₁₂	-e₃₁	-e₄₁	-e₄	-e₄₁₂	e₄₃₁	-e₃₂₁	-e₃	e₂	1	e₄₃	-e₄₂	-e₂₃	e₄₂₃
e₂	e₂	-e₁₂	1	e₂₃	-e₄₂	e₄₁₂	-e₄	-e₄₂₃	e₃	-e₃₂₁	-e₁	-e₄₃	1	e₄₁	-e₃₁	e₄₃₁
e₃	e₃	e₃₁	-e₂₃	1	-e₄₃	-e₄₃₁	e₄₂₃	-e₄	-e₂	e₁	-e₃₂₁	e₄₂	-e₄₁	1	-e₁₂	e₄₁₂
e₄	e₄	e₄₁	e₄₂	e₄₃	0	0	0	0	e₄₂₃	e₄₃₁	e₄₁₂	0	0	0	1	0
e₄₁	e₄₁	e₄	e₄₁₂	-e₄₃₁	0	0	0	0	-1	-e₄₃	e₄₂	0	0	0	-e₄₂₃	0
e₄₂	e₄₂	-e₄₁₂	e₄	e₄₂₃	0	0	0	0	e₄₃	-1	-e₄₁	0	0	0	-e₄₃₁	0
e₄₃	e₄₃	e₄₃₁	-e₄₂₃	e₄	0	0	0	0	-e₄₂	e₄₁	-1	0	0	0	-e₄₁₂	0
e₂₃	e₂₃	-e₃₂₁	-e₃	e₂	e₄₂₃	-1	-e₄₃	e₄₂	-1	-e₁₂	e₃₁	-e₄	-e₄₁₂	e₄₃₁	e₁	e₄₁
e₃₁	e₃₁	e₃	-e₃₂₁	-e₁	e₄₃₁	e₄₃	-1	-e₄₁	e₁₂	-1	-e₂₃	e₄₁₂	-e₄	-e₄₂₃	e₂	e₄₂
e₁₂	e₁₂	-e₂	e₁	-e₃₂₁	e₄₁₂	-e₄₂	e₄₁	-1	-e₃₁	e₂₃	-1	-e₄₃₁	e₄₂₃	-e₄	e₃	e₄₃
e₄₂₃	e₄₂₃	-1	-e₄₃	e₄₂	0	0	0	0	-e₄	-e₄₁₂	e₄₃₁	0	0	0	e₄₁	0
e₄₃₁	e₄₃₁	e₄₃	-1	-e₄₁	0	0	0	0	e₄₁₂	-e₄	-e₄₂₃	0	0	0	e₄₂	0
e₄₁₂	e₄₁₂	-e₄₂	e₄₁	-1	0	0	0	0	-e₄₃₁	e₄₂₃	-e₄	0	0	0	e₄₃	0
e₃₂₁	e₃₂₁	-e₂₃	-e₃₁	-e₁₂	-1	e₄₂₃	e₄₃₁	e₄₁₂	e₁	e₂	e₃	-e₄₁	-e₄₂	-e₄₃	-1	e₄
1	1	-e₄₂₃	-e₄₃₁	-e₄₁₂	0	0	0	0	e₄₁	e₄₂	e₄₃	0	0	0	-e₄	0

Transwedge Product

- In 4D algebra, we previously wrote

$$\mathbf{A} \frown \mathbf{B} = \mathbf{A} \wedge \mathbf{B} + \mathbf{A} \times \mathbf{B} + \mathbf{A} \cdot \tilde{\mathbf{B}}$$

- Now, we have something better:

$$\mathbf{A} \frown \mathbf{B} = \mathbf{A} \underset{0}{\frown} \mathbf{B} + \mathbf{A} \underset{1}{\frown} \mathbf{B} - \mathbf{A} \underset{2}{\frown} \mathbf{B}$$

$$= \mathbf{A} \wedge \mathbf{B} + \mathbf{A} \underset{1}{\frown} \mathbf{B} + \mathbf{A} \cdot \tilde{\mathbf{B}}$$

Transwedge Product

- This means that the geometric product is just another operation in the exterior algebra
- Every product / antiproduct in the exterior algebra, including the geometric product, can be derived from 3 primitive operations:
 - The wedge product \wedge
 - Taking of a complement $\bar{\mathbf{a}}$
 - Application of the metric $\mathbf{G}\mathbf{a}$

Transwedge Product

- Liminal products have geometric significance
- In 4D rigid algebra, one geometric combo conspicuously missing from our tables

Join Operation	Illustration
<p>Line containing points p and q.</p> $\mathbf{p} \wedge \mathbf{q} = (p_w q_x - p_x q_w) \mathbf{e}_{41} + (p_y q_z - p_z q_y) \mathbf{e}_{23} + (p_w q_y - p_y q_w) \mathbf{e}_{42} + (p_z q_x - p_x q_z) \mathbf{e}_{31} + (p_w q_z - p_z q_w) \mathbf{e}_{43} + (p_x q_y - p_y q_x) \mathbf{e}_{12}$	
<p>Plane containing line l and point p.</p> $\mathbf{l} \wedge \mathbf{p} = (l_{yy} p_z - l_{yz} p_y + l_{mx} p_w) \mathbf{e}_{423} + (l_{yz} p_x - l_{yx} p_z + l_{my} p_w) \mathbf{e}_{431} + (l_{yx} p_y - l_{yy} p_x + l_{mz} p_w) \mathbf{e}_{412} - (l_{mx} p_x + l_{my} p_y + l_{mz} p_z) \mathbf{e}_{321}$	

Meet Operation	Illustration
<p>Line where planes g and h intersect.</p> $\mathbf{g} \vee \mathbf{h} = (g_z h_y - g_y h_z) \mathbf{e}_{41} + (g_x h_w - g_w h_x) \mathbf{e}_{23} + (g_x h_z - g_z h_x) \mathbf{e}_{42} + (g_y h_w - g_w h_y) \mathbf{e}_{31} + (g_y h_x - g_x h_y) \mathbf{e}_{43} + (g_z h_w - g_w h_z) \mathbf{e}_{12}$	
<p>Point where plane g and line l intersect.</p> $\mathbf{g} \vee \mathbf{l} = (g_z l_{my} - g_y l_{mz} + g_w l_{vx}) \mathbf{e}_1 + (g_x l_{mz} - g_z l_{mx} + g_w l_{vy}) \mathbf{e}_2 + (g_y l_{mx} - g_x l_{my} + g_w l_{vz}) \mathbf{e}_3 - (g_x l_{vx} + g_y l_{vy} + g_z l_{vz}) \mathbf{e}_4$	

Expansion Operation	Illustration
<p>Line containing point p and orthogonal to plane g.</p> $\mathbf{p} \wedge \mathbf{g}^* = -p_w g_x \mathbf{e}_{41} + (p_z g_y - p_y g_z) \mathbf{e}_{23} - p_w g_y \mathbf{e}_{42} + (p_x g_z - p_z g_x) \mathbf{e}_{31} - p_w g_z \mathbf{e}_{43} + (p_y g_x - p_x g_y) \mathbf{e}_{12}$	
<p>Plane containing point p and orthogonal to line l.</p> $\mathbf{p} \wedge \mathbf{l}^* = -p_w l_{vx} \mathbf{e}_{423} - p_w l_{vy} \mathbf{e}_{431} - p_w l_{vz} \mathbf{e}_{412} + (p_x l_{vx} + p_y l_{vy} + p_z l_{vz}) \mathbf{e}_{321}$	
<p>Plane containing line l and orthogonal to plane g.</p> $\mathbf{l} \wedge \mathbf{g}^* = (l_{yy} g_z - l_{yz} g_y) \mathbf{e}_{423} + (l_{yz} g_x - l_{yx} g_z) \mathbf{e}_{431} + (l_{yx} g_y - l_{yy} g_x) \mathbf{e}_{412} - (l_{mx} g_x + l_{my} g_y + l_{mz} g_z) \mathbf{e}_{321}$	

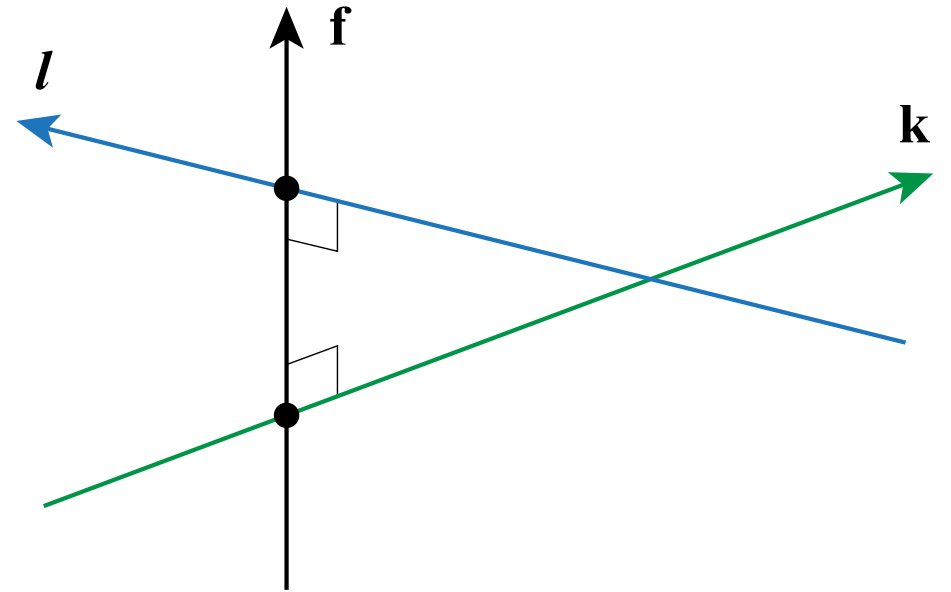
Transwedge Product

- Calculate line \mathbf{f} orthogonal to two skew lines l and k

$$\mathbf{f} = l \underset{1}{\vee} k$$

- Uses transwedge *antiproduct*
- Needs to be reconstrained so that

$$\mathbf{f}_v \cdot \mathbf{f}_m = 0$$



Transwedge Product

- \mathbf{f} will generally need to be “constrained” so that $\mathbf{f}_v \cdot \mathbf{f}_m = 0$
- This can be done by dividing by dual number $\sqrt{\mathbf{f} \vee \mathbf{f}}$
- Equivalent to Gram-Schmidt orthonormalization
- This dual number norm arises from isomorphism

$$\mathbb{R}^+(3, 0, 1) \cong \mathbb{D}^+(3, 0, 0)$$

Spacetime Geometric Algebra

- Add time dimension \mathbf{e}_0 that squares to -1

$$\mathbf{g} = \begin{bmatrix} -1 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 \end{bmatrix} \quad \begin{array}{l} \mathbf{e}_0 \cdot \mathbf{e}_0 = -1 \\ \mathbf{e}_1 \cdot \mathbf{e}_1 = +1 \\ \mathbf{e}_2 \cdot \mathbf{e}_2 = +1 \\ \mathbf{e}_3 \cdot \mathbf{e}_3 = +1 \\ \mathbf{e}_4 \cdot \mathbf{e}_4 = 0 \end{array}$$

Spacetime Geometric Algebra

- Position: $\mathbf{r} = ct\mathbf{e}_0 + x\mathbf{e}_1 + y\mathbf{e}_2 + z\mathbf{e}_3 + \mathbf{e}_4$

- Velocity: $\mathbf{u} = \frac{d\mathbf{r}}{d\tau} = \gamma c\mathbf{e}_0 + \gamma\dot{x}\mathbf{e}_1 + \gamma\dot{y}\mathbf{e}_2 + \gamma\dot{z}\mathbf{e}_3$

$$\gamma = \frac{dt}{d\tau} = \frac{1}{\sqrt{1 - u^2/c^2}}$$

Relativistic Quaternions

- Operators in 4D algebra transfer to 5D algebra through multiplication by \mathbf{e}_0

- Quaternion rotation: $\mathbf{q} = q_x \mathbf{e}_{410} + q_y \mathbf{e}_{420} + q_z \mathbf{e}_{430} + q_w \mathbb{1}$ $\mathbb{1} = \mathbf{e}_{01234}$

$$\mathbf{q}(\tau) = (a_x \mathbf{e}_{410} + a_y \mathbf{e}_{420} + a_z \mathbf{e}_{430}) \sin\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) + \mathbb{1} \cos\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) \quad \dot{\phi} = d\phi/dt$$

$$\mathbf{q}(\tau) = \exp_{\vee}\left(\frac{1}{2} \gamma \tau \dot{\phi} \mathbf{l}\right) \quad \mathbf{l} = a_x \mathbf{e}_{410} + a_y \mathbf{e}_{420} + a_z \mathbf{e}_{430}$$

Relativistic Quaternions

- Sandwich product $\mathbf{q}(\tau) \vee \mathbf{r} \vee \tilde{\mathbf{q}}(\tau)$ performs an instantaneous rotation
- Any physically meaningful motion must happen over some amount of time
- Also must respect speed of light

Relativistic Quaternions

- General translation operator:

$$\mathbf{T}(\tau) = \frac{1}{2} \gamma \tau (-c \mathbf{e}_{321} + \dot{x} \mathbf{e}_{230} + \dot{y} \mathbf{e}_{310} + \dot{z} \mathbf{e}_{120}) + \mathbb{1}$$

- Strictly temporal translation:

$$\mathbf{S}(\tau) = \mathbb{1} - \frac{1}{2} \gamma c \tau \mathbf{e}_{321}$$

Relativistic Quaternions

- Combine rotation and temporal translation:

$$\mathbf{Q}(\tau) = \mathbf{q}(\tau) \vee \left(\mathbb{1} - \frac{1}{2} \gamma c \tau \mathbf{e}_{321} \right)$$

$$\begin{aligned} \mathbf{Q}(\tau) = & \left(a_x \mathbf{e}_{410} + a_y \mathbf{e}_{420} + a_z \mathbf{e}_{430} \right) \sin \left(\frac{1}{2} \gamma \tau \dot{\phi} \right) + \mathbb{1} \cos \left(\frac{1}{2} \gamma \tau \dot{\phi} \right) \\ & - \frac{1}{2} \gamma c \tau \left(a_x \mathbf{e}_1 + a_y \mathbf{e}_2 + a_z \mathbf{e}_3 \right) \sin \left(\frac{1}{2} \gamma \tau \dot{\phi} \right) - \frac{1}{2} \gamma c \tau \mathbf{e}_{321} \cos \left(\frac{1}{2} \gamma \tau \dot{\phi} \right) \end{aligned}$$

Relativistic Quaternions

- Set $\tau = t/\gamma$
 - Then $\mathbf{q}(\tau) \vee \mathbf{r} \vee \mathbf{q}(\tau)$ rotates \mathbf{r} through angle $\dot{\phi}t$ and adds ct to the time coordinate
 - Generically, s coordinates are q coordinates times $-\frac{1}{2}\gamma c\tau$
- $$\mathbf{Q} = q_x \mathbf{e}_{410} + q_y \mathbf{e}_{420} + q_z \mathbf{e}_{430} + q_w \mathbf{1} + s_x \mathbf{e}_1 + s_y \mathbf{e}_2 + s_z \mathbf{e}_3 + s_w \mathbf{e}_{321}$$

Relativistic Quaternions

- Operator **Q** is equivalent to 5 x 5 matrix

$$\mathbf{m} = \begin{bmatrix} 1 & 0 & 0 & 0 & -2(q_x s_x + q_y s_y + q_z s_z + q_w s_w) \\ 0 & 1 - 2q_y^2 - 2q_z^2 & 2(q_x q_y - q_w q_z) & 2(q_z q_x + q_w q_y) & 0 \\ 0 & 2(q_x q_y + q_w q_z) & 1 - 2q_z^2 - 2q_x^2 & 2(q_y q_z - q_w q_x) & 0 \\ 0 & 2(q_z q_x - q_w q_y) & 2(q_y q_z + q_w q_x) & 1 - 2q_x^2 - 2q_y^2 & 0 \\ 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

Relativistic Quaternions

- Motor (dual quaternion) from 4D algebra becomes

$$\mathbf{d}(\tau) = \mathbf{l} \sin\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) + \mathbb{1} \cos\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) - \left(\frac{1}{2} \gamma \tau \dot{\mathbf{l}}^{\star} \wedge \mathbf{e}_0\right) \cos\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) - \frac{1}{2} \gamma \tau \dot{\mathbf{e}}_0 \sin\left(\frac{1}{2} \gamma \tau \dot{\phi}\right)$$

- Again multiply by temporal translation

$$\mathbf{D}(\tau) = \mathbf{d}(\tau) \vee \left(\mathbb{1} - \frac{1}{2} \gamma c \tau \mathbf{e}_{321} \right)$$

Relativistic Quaternions

$$\mathbf{D}(\tau) = \mathbf{l} \sin\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) + \mathbb{1} \cos\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) - \left(\frac{1}{2} \gamma \tau \dot{\delta} \mathbf{l}^{\star} \wedge \mathbf{e}_0\right) \cos\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) - \frac{1}{2} \gamma \tau \dot{\delta} \mathbf{e}_0 \sin\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) \\ - \frac{1}{2} \gamma c \tau \left[\mathbf{l} \sin\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) + \mathbb{1} \cos\left(\frac{1}{2} \gamma \tau \dot{\phi}\right) \right] \vee \mathbf{e}_{321}$$

$$\mathbf{D} = q_x \mathbf{e}_{410} + q_y \mathbf{e}_{420} + q_z \mathbf{e}_{430} + q_w \mathbb{1} + m_x \mathbf{e}_{230} + m_y \mathbf{e}_{310} + m_z \mathbf{e}_{120} + m_w \mathbf{e}_0 \\ + s_x \mathbf{e}_1 + s_y \mathbf{e}_2 + s_z \mathbf{e}_3 + s_w \mathbf{e}_{321}$$

Relativistic Quaternions

- Assuming weight one, norm of a relativistic dual quaternion is

$$\|\mathbf{D}\|_{\bullet} = \sqrt{\mathbf{D} \cdot \mathbf{D}} = \sqrt{s_x^2 + s_y^2 + s_z^2 + s_w^2 - m_x^2 - m_y^2 - m_z^2 - m_w^2}$$

- $m_x^2 + m_y^2 + m_z^2 + m_w^2$ is square of half the distance a particle starting at the origin is moved by \mathbf{D} through space
- $s_x^2 + s_y^2 + s_z^2 + s_w^2 = \frac{1}{4} \gamma^2 c^2 \tau^2$ is square of half the distance through time

Relativistic Quaternions

- Norm is real precisely when particle moves at less than or equal to the speed of light

$$\|\mathbf{D}\|_{\bullet} = \sqrt{\mathbf{D} \cdot \mathbf{D}} = \sqrt{s_x^2 + s_y^2 + s_z^2 + s_w^2 - m_x^2 - m_y^2 - m_z^2 - m_w^2}$$

Relativistic Quaternions

- Setting $\dot{\phi} = 0$, \mathbf{D} reduces to translation operator with norm

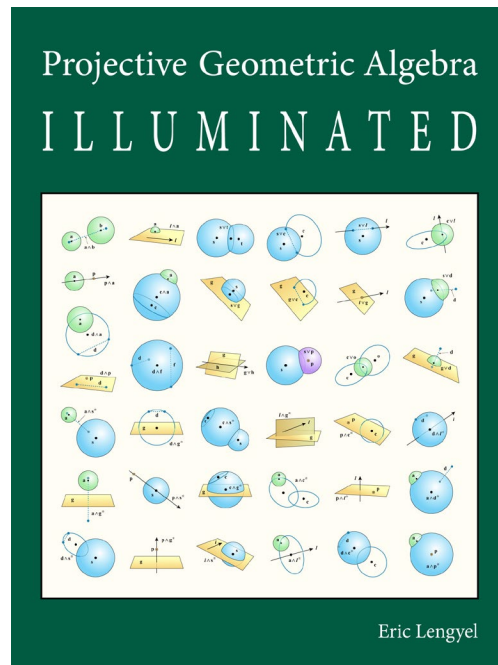
$$\|\mathbf{T}(\tau)\|_{\bullet} = \frac{1}{2} \gamma \tau \sqrt{c^2 - \dot{x}^2 - \dot{y}^2 - \dot{z}^2}$$

- Setting $dt = \gamma \tau$, $dx = \dot{x} dt$, $dy = \dot{y} dt$, and $dz = \dot{z} dt$,

$$\|\mathbf{T}(\tau)\|_{\bullet} = \frac{1}{2} \sqrt{c^2 dt^2 - dx^2 - dy^2 - dz^2}$$

References

- Projective Geometric Algebra Illuminated
- projectivegeometricalgebra.org



Projective Geometric Algebra

projectivegeometricalgebra.org

Unary Operations	Binary Operations	Scalars	Transformation Groups																																																																																																							
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